

RF PA 1.5A DC/DC Regulator

ISL9109 is 1.6MHz synchronous step-down regulator with integrated power switches capable of delivering 1.5A output for powering RF Power Amplifiers in cellular phones. The ISL9109 features a standby mode which allows for rapid startup while prolonging battery life. The supply voltage range is from 2.7V to 5.5V allowing the use of a single Li+ cell, three NiMH cells, or a regulated 5V input. 1.6MHz pulse-width modulation (PWM) switching frequency allows using small external components. It has a flexible operation mode selection of forced PWM mode and Skip (Low I_Q) mode with typical 22µA quiescent current for highest light load efficiency to maximize battery life.

The ISL9109 integrates a pair of low ON-resistance P-Channel and N-Channel MOSFETs to maximize efficiency and minimize external component count.

When in standby, the ISL9109 band-gap reference is powered. This assists in a rapid power-up when the EN pin is asserted high. Other features include soft-start, overcurrent protection, and thermal shutdown.

The ISL9109 is offered in 8 Ld 2mmx3mm DFN package with 0.9mm typical height. The complete converter can occupy less than 1cm² area.

Ordering Information

PART NUMBER (Note)	PART MARKING	TEMP. RANGE (°C)	PACKAGE (Pb-free)	PKG. DWG. #
ISL9109IRZ*	109	-40 to +85	8 Ld 2x3 DFN	L8.2x3

*Add "-T" suffix for tape and reel. Please refer to TB347 for details on reel specifications.

NOTE: These Intersil Pb-free plastic packaged products employ special Pb-free material sets, molding compounds/die attach materials, and 100% matte tin plate plus anneal (e3 termination finish, which is RoHS compliant and compatible with both SnPb and Pb-free soldering operations). Intersil Pb-free products are MSL classified at Pb-free peak reflow temperatures that meet or exceed the Pb-free requirements of IPC/JEDEC J STD-020.

Features

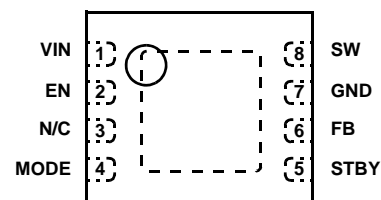
- Integrated Synchronous Buck Regulator with up to 95% Efficiency
- 2.7V to 5.5V Supply Voltage
- 1.5A Output Current
- 4.3µA Quiescent Supply Current in Standby Mode
- 22µA Quiescent Supply Current in Skip (Low I_Q) Mode
- 3% Output Accuracy Over Temperature/Load/Line
- Selectable Forced PWM Mode or Skip Mode
- Less Than 1µA Logic Controlled Shutdown Current
- 100% Maximum Duty Cycle for Lowest Dropout
- Soft-Start
- Peak Current Limiting, Short Circuit Protection
- Over-Temperature Protection
- 8 Ld 2mmx3mm DFN
- Pb-Free (RoHS Compliant)

Applications

- Single Li-Ion Battery-Powered Equipment
- RF Power Amplifier
- CPU Power
- PDAs and Palmtops

Pinout

ISL9109
(8 LD 2X3 DFN)
TOP VIEW



Absolute Maximum Ratings (Reference to GND)

VIN	-0.3V to 6.5V
EN, MODE, STBY	-0.3V to VIN + 0.3V
SW	-1.5V to 6.5V
FB	-0.3V to 2.7V

Thermal Information

Thermal Resistance (Notes 1, 2)	θ_{JA} (°C/W)	θ_{JC} (°C/W)
2x3 DFN Package	55	5.5
Junction Temperature Range	-40°C to +125°C	
Storage Temperature Range	-65°C to +150°C	
Pb-Free Reflow Profile	see link below	
http://www.intersil.com/pbfree/Pb-FreeReflow.asp		

Recommended Operating Conditions

VIN Supply Voltage Range	2.7V to 5.5V
Load Current	0A to 1.5A
Ambient Temperature Range	-40°C to +85°C

CAUTION: Do not operate at or near the maximum ratings listed for extended periods of time. Exposure to such conditions may adversely impact product reliability and result in failures not covered by warranty.

NOTES:

- θ_{JA} is measured in free air with the component mounted on a high effective thermal conductivity test board with “direct attach” features. See Tech Brief TB379.
- θ_{JC} , “case temperature” location is at the center of the exposed metal pad on the package underside. See Tech Brief TB379.

Electrical Specifications Unless otherwise noted, all parameter limits are guaranteed over the recommended operating conditions and the typical specifications are measured at the following conditions: $T_A = +25^\circ\text{C}$, $V_{IN} = V_{EN} = 3.6\text{V}$, $L = 2.2\mu\text{H}$, $C_1 = 10\mu\text{F}$, $C_2 = 10\mu\text{F}$, $I_{OUT} = 0\text{A}$ (see the “Typical Applications” on page 7).

PARAMETER	SYMBOL	TEST CONDITIONS	MIN	TYP	MAX	UNITS
SUPPLY						
Undervoltage Lockout Threshold	V_{UVLO}	Rising	-	2.5	2.7	V
		Falling	2.2	2.4	-	V
Quiescent Supply Current	I_{VIN}	EN = STBY = LOW (Shut Down) $T_A = +25^\circ\text{C}$	-	0.05	2	μA
		EN = STBY = HI for $\geq 1\text{ms}$, then EN = LOW, STBY = HI (Standby) $T_A = +25^\circ\text{C}$	-	4.3	6.0	μA
		EN = MODE = HI, no load at the output	-	22	30	μA
		EN = HI, MODE = LOW, no load at the output, VFB = 0.75V	-	3.6	5.5	mA
OUTPUT REGULATION						
FB Regulation Voltage	V_{FB}	MODE = LOW	0.78	0.8	0.82	V
FB Bias Current	I_{FB}	VFB = 0.75V	-	0.1	-	μA
Line Regulation		$V_{IN} = V_O + 0.5\text{V}$ to 5.5V (minimal 2.7V)	-	0.2	-	%/V
COMPENSATION						
Error Amplifier Trans-conductance		Design info only	-	20	-	$\mu\text{A/V}$
SW						
P-Channel MOSFET ON-resistance		$V_{IN} = 3.6\text{V}$, $I_O = 200\text{mA}$	-	0.12	0.22	Ω
		$V_{IN} = 2.7\text{V}$, $I_O = 200\text{mA}$	-	0.16	0.27	Ω
N-Channel MOSFET ON-resistance		$V_{IN} = 3.6\text{V}$, $I_O = 200\text{mA}$	-	0.11	0.22	Ω
		$V_{IN} = 2.7\text{V}$, $I_O = 200\text{mA}$	-	0.15	0.27	Ω
P-Channel MOSFET Peak Current Limit	I_{PK}	$V_{IN} = 5.5\text{V}$, $L = 3.3\mu\text{H}$, V_{OUT} shorted to GND thru a 50m Ω resistor	1.8	2.1	2.6	A
Maximum Duty Cycle			-	100	-	%
PWM Switching Frequency	f_S		1.35	1.6	1.75	MHz
SW Minimum On Time		MODE = LOW (forced PWM mode)	-	80	-	ns

Electrical Specifications

Unless otherwise noted, all parameter limits are guaranteed over the recommended operating conditions and the typical specifications are measured at the following conditions: $T_A = +25^\circ\text{C}$, $V_{IN} = V_{EN} = 3.6\text{V}$, $L = 2.2\mu\text{H}$, $C_1 = 10\mu\text{F}$, $C_2 = 10\mu\text{F}$, $I_{OUT} = 0\text{A}$ (see the "Typical Applications" on page 7). **(Continued)**

PARAMETER	SYMBOL	TEST CONDITIONS	MIN	TYP	MAX	UNITS
Soft Start-Up Time	t_{SS}	STBY = 0, EN = $_$	-	1.1	-	ms
		Start-Up is considered complete when V_{OUT} reaches 93% of final target voltage.				
		STBY = 1 for $\geq 1\text{mS}$, EN = $_$	-	-	60	μs
		Start-up is considered complete when V_{OUT} reaches 93% of final target voltage.				
STBY, EN, MODE						
Logic Input Low			-	-	0.4	V
Logic Input High			1.4	-	-	V
Logic Input Leakage Current		Pulled up to 5.5V	-	0.1	1	μA
THERMAL SHUTDOWN						
Thermal Shutdown			-	160	-	$^\circ\text{C}$
Thermal Shutdown Hysteresis			-	25	-	$^\circ\text{C}$

Pin Descriptions

PIN #	PIN NAME	DESCRIPTION
1	VIN	Input supply voltage. Connect a 10 μF ceramic capacitor to power ground.
2	EN	Enable pin. Enable the output when driven to high. Shut down the chip and discharge output capacitor when driven to low. Do not leave this pin floating
3	N/C	Do not connect; leave floating for proper device operation
4	MODE	Mode selection pin. Connect to logic high or VIN to enable skip mode; connect to logic low or ground for force PWM mode.
5	STBY	Active high enables the band-gap reference.
6	FB	Buck regulator output feedback pin. Connect to the output voltage through voltage divider resistors for adjustable output voltage.
7	GND	System ground.
8	SW	Switching node connection. Connect to one terminal of the inductor.
E-PAD	-	Exposed pad. It should be connected to ground for proper electrical performance. For best thermal performance, connect as much copper as possible to this pad, either on the component layer or other layers through thermal vias.

Typical Operating Performance

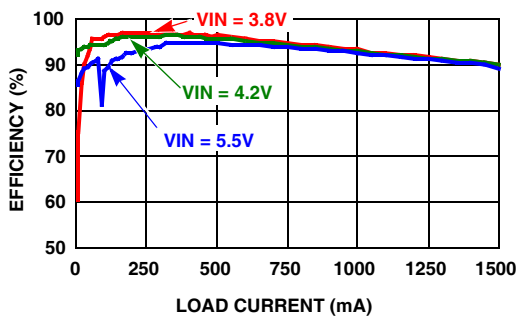


FIGURE 1. EFFICIENCY vs LOAD CURRENT ($V_{OUT} = 3.3\text{V}$)

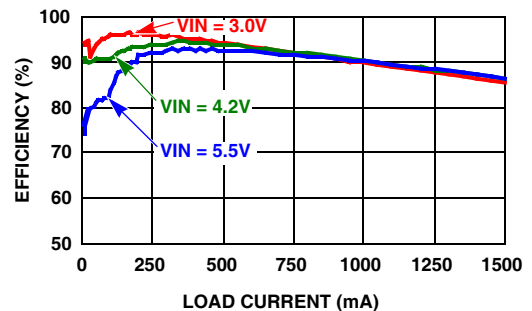


FIGURE 2. EFFICIENCY vs LOAD CURRENT ($V_{OUT} = 2.5\text{V}$)

Typical Operating Performance (Continued)

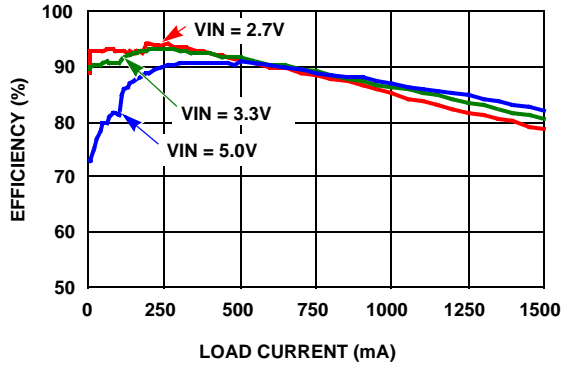


FIGURE 3. EFFICIENCY vs LOAD CURRENT ($V_{OUT} = 1.8V$)

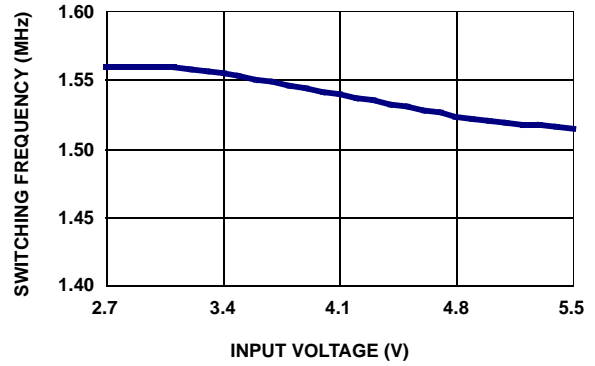


FIGURE 4. SWITCHING FREQUENCY vs INPUT VOLTAGE, ($V_{OUT} = 1.6V$, $I_{OUT} = 1A$, $T_A = +25^{\circ}C$)

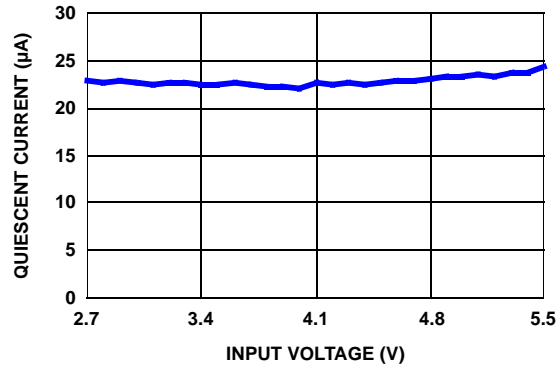


FIGURE 5. I_Q vs V_{IN} (MODE = V_{IN} , STBY = V_{IN} , EN = V_{IN} , $V_{OUT} = 1.6V$, $I_{OUT} = 0$)

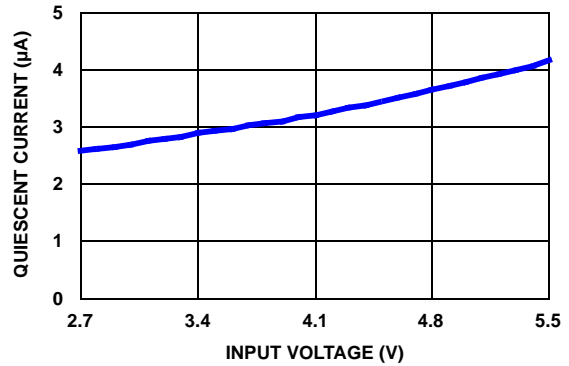


FIGURE 6. I_Q vs V_{IN} (MODE = V_{IN} , STBY = V_{IN} , EN = GND, $I_{OUT} = 0$)

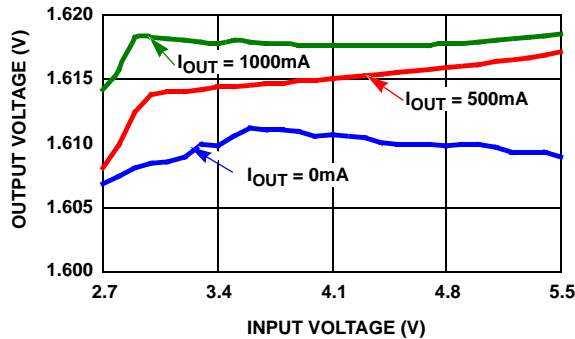


FIGURE 7. V_{OUT} vs V_{IN} (MODE = V_{IN} , $V_{OUT} = 1.6V$)

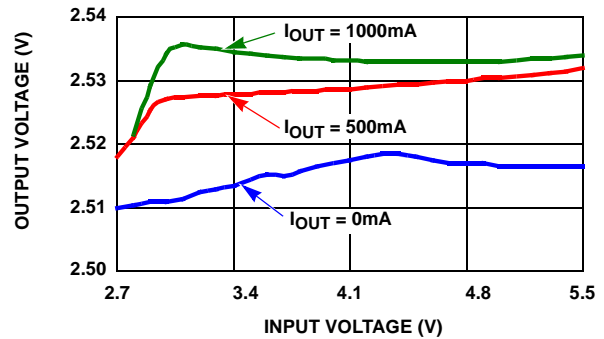


FIGURE 8. V_{OUT} vs V_{IN} (MODE = V_{IN} , $V_{OUT} = 2.5V$)

Typical Operating Performance (Continued)

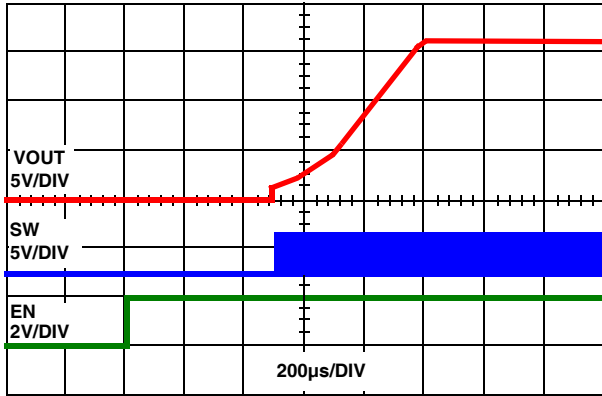


FIGURE 9. SOFT-START ($V_{IN} = 4.2V$, $V_{OUT} = 1.6V$, $STBY = 0V$, $I_{OUT} = 500mA$)

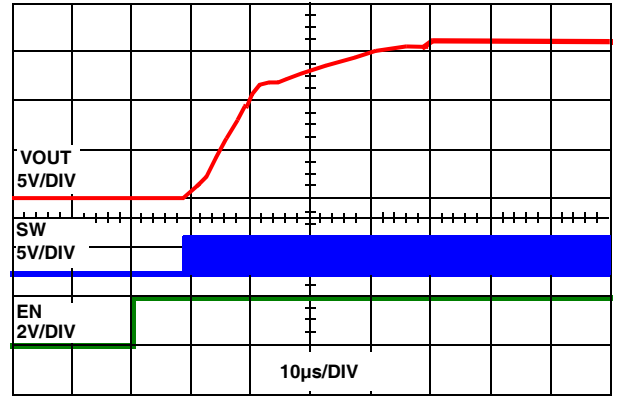


FIGURE 10. SOFT-START ($V_{IN} = 4.2V$, $V_{OUT} = 1.6V$, $STBY = V_{IN}$, $I_{OUT} = 500mA$)

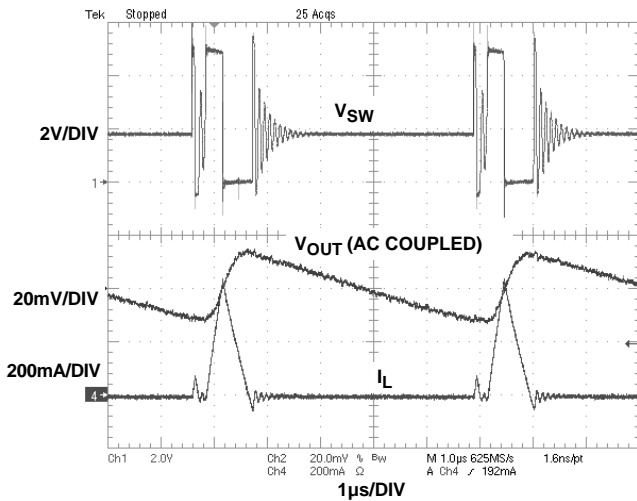


FIGURE 11. STEADY-STATE IN SKIP MODE ($V_{IN} = 5.0V$, $V_{OUT} = 1.8V$, $I_{OUT} = 35mA$)

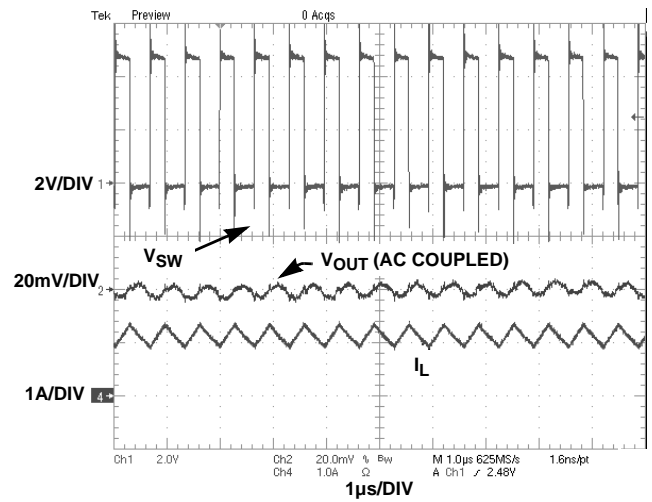


FIGURE 12. STEADY-STATE IN PWM MODE ($V_{IN} = 5.0V$, $V_{OUT} = 1.8V$, $I_{OUT} = 1.2A$)

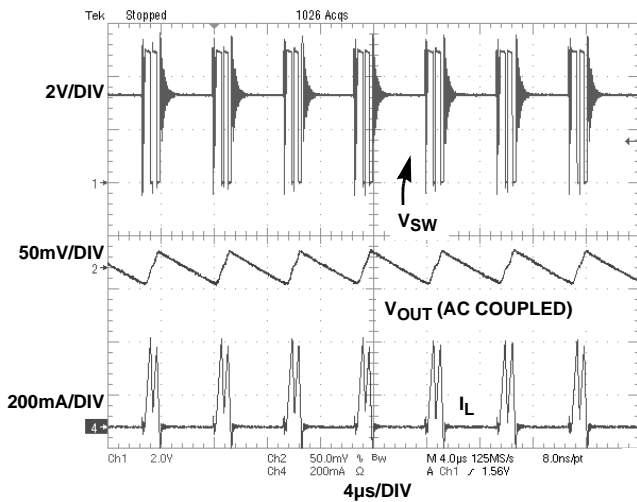


FIGURE 13. STEADY-STATE IN SKIP MODE ($V_{IN} = 5.0V$, $V_{OUT} = 3.3V$, $I_{OUT} = 35mA$)

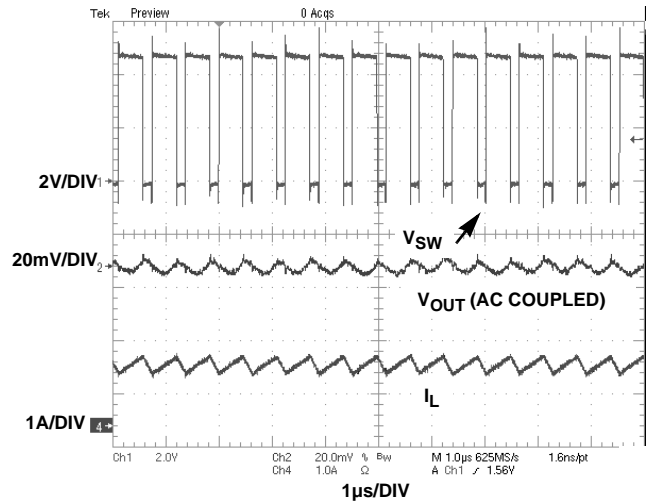


FIGURE 14. STEADY-STATE IN PWM MODE ($V_{IN} = 5.0V$, $V_{OUT} = 3.3V$, $I_{OUT} = 1.2A$)

Typical Operating Performance (Continued)

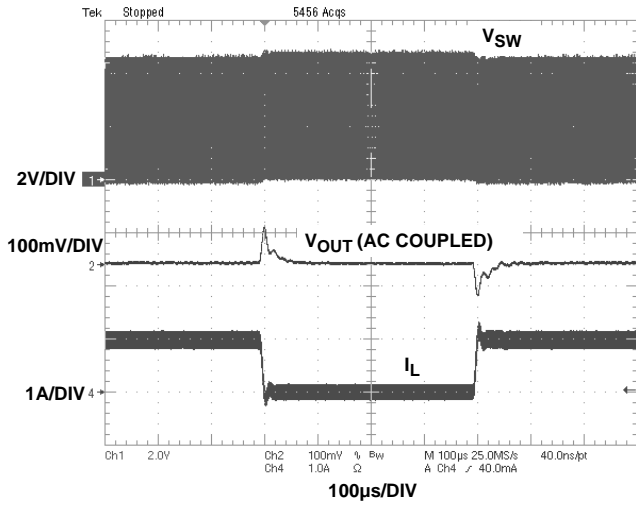


FIGURE 15. LOAD TRANSIENT TEST (MODE=GND $V_{IN} = 5.0V$; $V_O = 1.5V$; $I_O = 0.01A\sim 1A$)

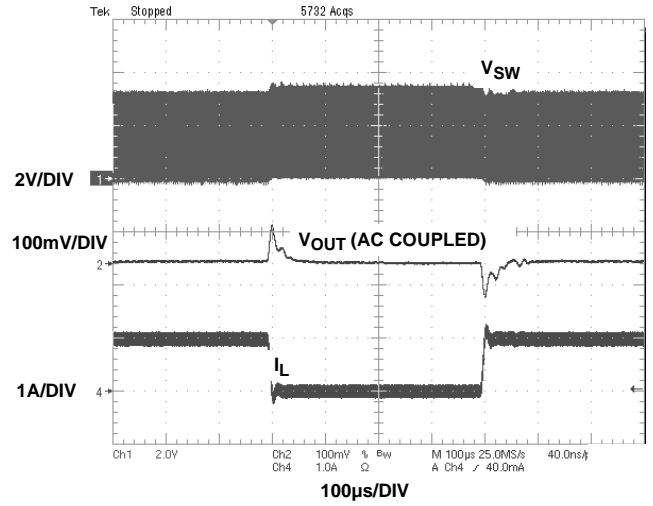


FIGURE 16. LOAD TRANSIENT TEST (MODE = GND, $V_{IN} = 3.6V$; $V_O = 1.5V$; $I_O = 0.01A\sim 1A$)

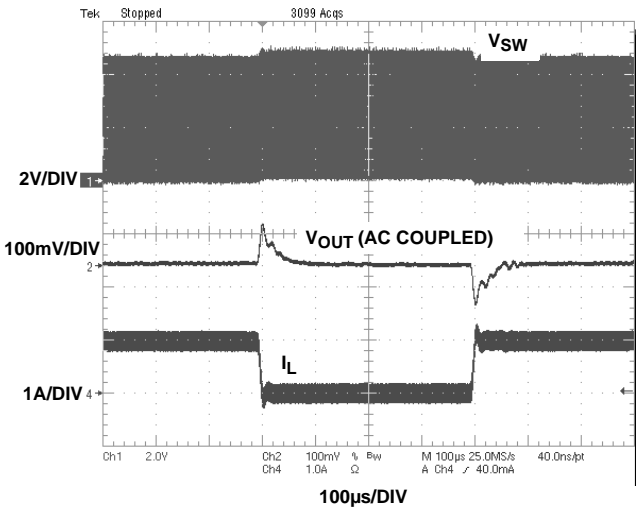


FIGURE 17. LOAD TRANSIENT TEST (MODE = GND, $V_{IN} = 3.6V$; $V_O = 2.5V$; $I_O = 0.01A\sim 1A$)

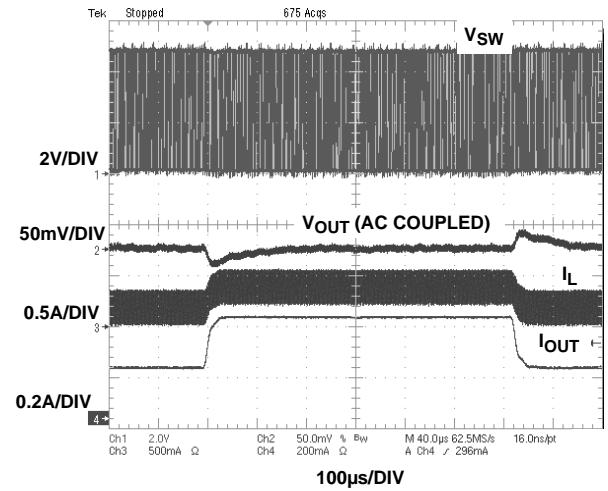
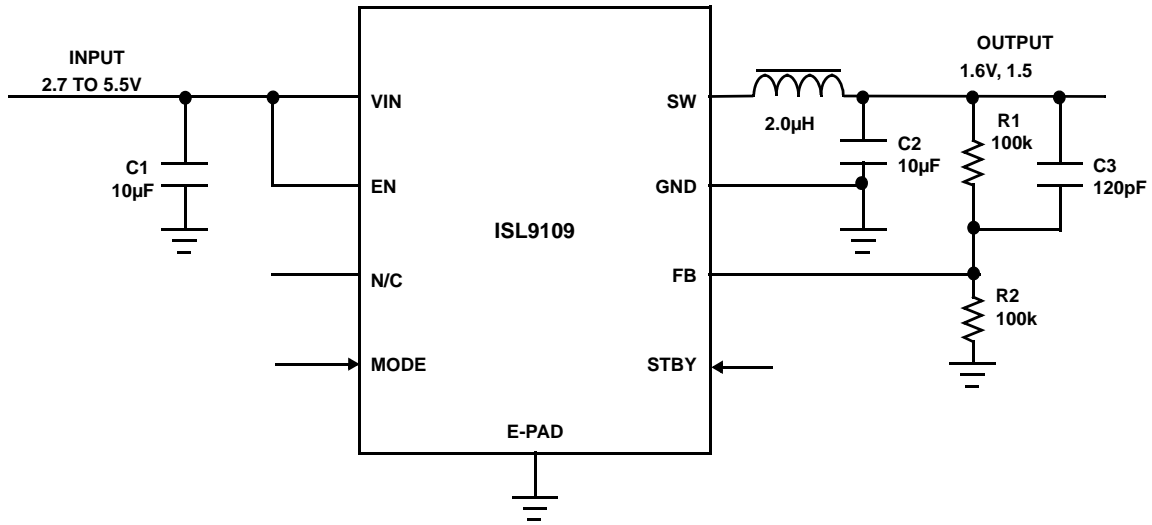


FIGURE 18. LOAD TRANSIENT TEST (MODE = $V_{IN} = 5V$; $V_O = 3.3V$; $I_O = 0.2A\sim 0.4A$)

Typical Applications



PARTS	DESCRIPTION	MANUFACTURERS	PART NUMBER	SPECIFICATIONS	SIZE
L	Inductor	Toko	1098AS-2R0AM	2.0µH/1.8A/67mΩ	3.0mmx3.2mmx1.2mm
C ₁	Input capacitor	Murata	GRM21BR60J106KE19L	10µF/6.3V	2.0mmx1.25mmx1.25mm
C ₂	Output capacitor	Murata	GRM21BR60J106KE19L	10µF/6.3V	2.0mmx1.25mmx1.25mm
C ₃	Capacitor	Murata	GRM1885C1H121JA01D	120pF/50V	1.6mmx0.8mmx0.8mm
R ₁ , R ₂	Resistor	Various		100kΩ, SMD, 0.5%	1.6mmx0.8mmx0.45mm

FIGURE 19. TYPICAL APPLICATION DIAGRAM

Theory of Operation

The ISL9109 is a step-down switching regulator optimized for battery-powered handheld applications. The regulator operates at a typical 1.6MHz fixed switching frequency under heavy load conditions to allow small external inductor and capacitors to be used for minimal printed-circuit board (PCB) area. At light load, the regulator can be selected to enter skip mode to reduce the switching frequency. Unless forced to the fixed frequency, to minimize the switching loss and to maximize the battery life. The quiescent current under skip mode, with no loading is typically only 22 μ A. The supply current is typically only 4 μ A in standby mode, and 0.05 μ A when the regulator is in shutdown mode.

PWM Control Scheme

The device uses the peak-current mode pulse-width modulation (PWM) control scheme for fast transient response and pulse-by-pulse current limiting. Figure 20 shows the circuit functional block diagram. The current loop consists of the oscillator, the PWM comparator COMP, current sensing circuit, and the slope compensation for the current loop stability. The current sensing circuit consists of the resistance of the P-Channel MOSFET when it is turned on, and the Current Sense Amplifier (CSA). The control reference for the current loops comes from the Error Amplifier (EAMP) of the voltage loop.

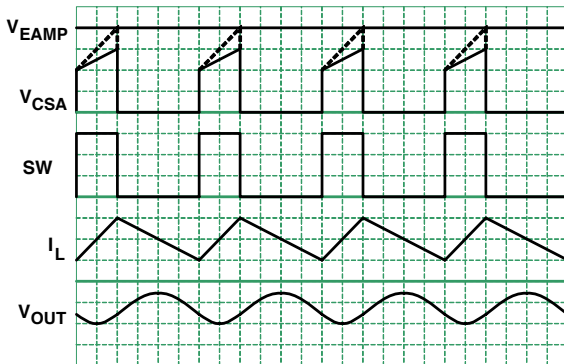


FIGURE 21. PWM OPERATION WAVEFORMS

The PWM operation is initialized by the clock from the oscillator. The P-Channel MOSFET is turned on at the beginning of a PWM cycle and the current in the P-Channel MOSFET starts ramping up. When the sum of the CSA output and the compensation slope reaches the control reference of the current loop, the PWM comparator COMP sends a signal to the PWM logic to turn off the P-Channel MOSFET and to turn on the N-Channel MOSFET. The N-MOSFET remains on until the end of the PWM cycle. Figure 21 shows the typical operating waveforms during the normal PWM operation. The dotted lines illustrate the sum of the slope compensation ramp and the CSA output.

The output voltage is regulated by controlling the reference voltage to the current loop. The band-gap circuit outputs a 0.8V reference voltage to the voltage control loop. The

feedback signal comes from the FB pin. The soft-start block only affects the operation during the start-up and will be discussed separately in “Soft Start-Up” on page 10. The EAMP is a trans conductance amplifier, which converts the voltage error signal to a current output. The voltage loop is internally compensated by a RC network. The maximum EAMP voltage output is precisely clamped to the band-gap voltage.

Skip Mode

With the MODE pin connected to logic high, the device enters a pulse-skipping mode at light load to minimize the switching loss by reducing the switching frequency. Figure 22 illustrates the skip mode operation. A zero-cross sensing circuit (as shown in Figure 20) monitors the N-Channel MOSFET current for zero crossing. When it is detected to cross zero for 8 consecutive cycles, the regulator enters the skip mode. During the 8 consecutive cycles, the inductor current could be negative. The counter is reset to zero when the sensed N-Channel MOSFET current does not cross zero during any cycle within the 8 consecutive cycles. Once the device enters the skip mode, the pulse modulation starts being controlled by the SKIP comparator shown in Figure 20. Each pulse cycle is still synchronized by the PWM clock. The P-Channel MOSFET is turned on at the rising edge of clock and turned off when its current reaches 20% of the peak current limit. As the average inductor current in each cycle is higher than the average current of the load, the output voltage rises cycle over cycle. When the output voltage reaches 1.5% above its nominal voltage, the P-Channel MOSFET is turned off immediately and the inductor current is fully discharged to zero and stays at zero. The output voltage reduces gradually due to the load current discharging the output capacitor. When the output voltage drops to the nominal voltage, the P-Channel MOSFET will be turned on again, repeating the previous operations.

The regulator switches to PWM mode operation when the output voltage is sensed to drop below 1.5% of its nominal voltage value.

Enable

The enable (EN) pin allows user to enable or disable the converter for purposes such as power-up sequencing. With the EN pin pulled to high, the converter is enabled and the internal reference circuit wakes up first, and then the soft start-up begins. When the EN pin is pulled to logic low, the converter is disabled, the P-Channel MOSFET is turned off immediately, and the output capacitor is discharged through internal discharge path.

Undervoltage Lockout (UVLO)

When the input voltage is below the Undervoltage Lock Out (UVLO) threshold, the device is disabled.

Mode Selection

The MODE pin is provided on ISL9109 to select the operation mode. When it is driven to logic low or ground, the regulator operates in forced PWM mode. Under forced PWM mode, the device remains at the fixed PWM operation (typical at 1.6MHz), regardless of if the load current is high or low.

When the MODE pin is driven to logic high or connected to input voltage V_{IN} , the regulator operates in either SKIP mode or fixed PWM mode depending on the different load conditions.

Overcurrent Protection

The overcurrent protection is provided when over load condition happens. It is realized by monitoring the CSA output with the OCP comparator, as shown in Figure 20. When the current at P-Channel MOSFET is sensed to reach the current limit, the OCP comparator is triggered to turn off the P-Channel MOSFET immediately.

Short-Circuit Protection

As shown in Figure 20, the device has a Short-Circuit Protection (SCP) comparator, which monitors the FB pin voltage for output short-circuit protection. When the FB voltage is lower than 0.2V, the SCP comparator forces the PWM oscillator frequency to drop to 1/3 of its normal operation frequency.

Soft Start-Up

The soft-start-up eliminates the inrush current during the circuit start-up. The soft-start block outputs a ramp reference to both the voltage loop and the current loop. The two ramps limit the inductor current rising speed as well as the output voltage speed so that the output voltage rises in a controlled fashion. At the very beginning of the start-up, the output voltage is less than 0.2V; hence the PWM operating frequency is 1/3 of the normal frequency.

Power MOSFETs

The power MOSFETs are optimized to achieve better efficiency. The ON-resistance for the P-Channel MOSFET is typically 0.16Ω and the typical ON-resistance for the N-Channel MOSFET is 0.15Ω .

Low Dropout Operation

The ISL9109 features low dropout operation to maximize the battery life. When the input voltage drops to a level that the device can no longer operate under switching regulation to maintain the output voltage, the P-Channel MOSFET is completely turned on (100% duty cycle). The dropout voltage under such condition is the product of the load current and the ON-resistance of the P-Channel MOSFET. Minimum required input voltage V_{IN} under this condition is the sum of output voltage plus the voltage drop across the inductor and the P-Channel MOSFET switch.

Thermal Shut Down

The ISL9109 provides built-in thermal protection function. The thermal shutdown threshold temperature is typical $+160^{\circ}\text{C}$ with typical $+25^{\circ}\text{C}$ hysteresis. When the internal temperature is sensed to reach $+150^{\circ}\text{C}$, the regulator is completely shut down and as the temperature is sensed to drop to $+125^{\circ}\text{C}$ (typical), the device resumes operation starting from the soft-start-up.

STBY

The ISL9109 STBY pin enables the band-gap reference. This provides a method to quickly start up the buck regulator and ensure the output voltage reaches 93% of its nominal value within $60\mu\text{s}$ when the EN pin is asserted. The band-gap takes typical $600\mu\text{s}$ to bias up and stabilize. By asserting STBY high at least 1ms prior to asserting the EN, the device can provide a stable output when needed. A detailed timing diagram is shown in Figure 23.

Standby mode is entered by asserting the EN pin low while STBY pin is high. To achieve the specified standby operating current, both EN and STBY pins must be asserted high for at least 1ms after circuit start-up, before placing the device in standby mode.

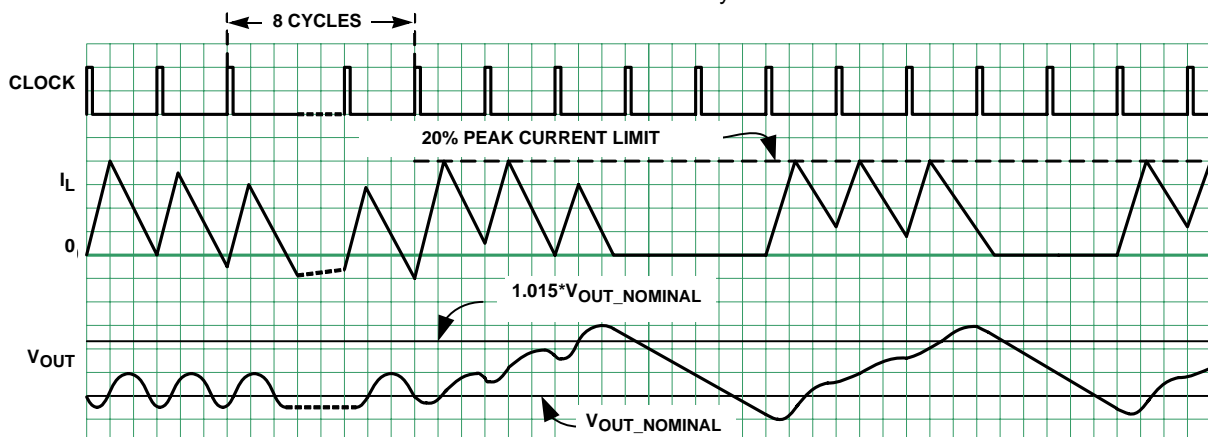


FIGURE 22. SKIP MODE OPERATION WAVEFORMS

Applications Information

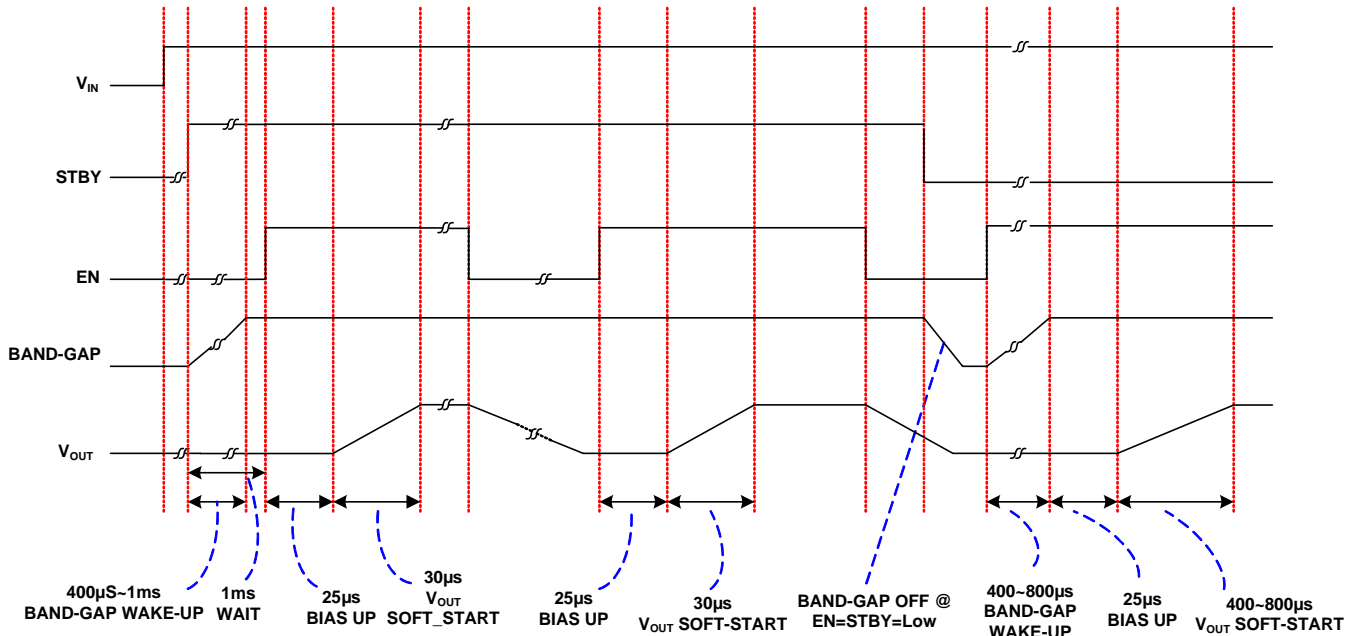


FIGURE 23. TIMING DIAGRAM

Inductor and Output Capacitor Selection

To achieve better steady state and transient response, typically a 2.2µH inductor can be used. The peak-to-peak inductor current ripple can be expressed as follows in Equation 1:

$$\Delta I = \frac{V_O \cdot \left(1 - \frac{V_O}{V_{IN}}\right)}{L \cdot f_S} \quad (\text{EQ. 1})$$

In Equation 1, usually the typical values can be used but to have a more conservative estimation; the inductance should consider the value with worst case tolerance. For switching frequency f_S , the minimum f_S from the “Electrical Specifications” table on page 2 can be used.

To select the inductor, its saturation current rating should be at least higher than the sum of the maximum output current and half of the delta calculated from Equation 1. Another more conservative approach is to select the inductor with the current rating higher than the P-Channel MOSFET peak current limit.

Another consideration is the inductor DC resistance since it directly affects the efficiency of the converter. Ideally, the inductor with the lower DC resistance should be considered to achieve higher efficiency.

Inductor specifications could be different from different manufacturers so please check with each manufacturer if additional information is needed.

For the output capacitor, a ceramic capacitor can be used because of the low ESR values, which helps to minimize the output voltage ripple. A typical value of 10µF/6.3V ceramic capacitor should be enough for most of the applications and the capacitor should be X5R or X7R.

Input Capacitor Selection

The main function for the input capacitor is to provide decoupling of the parasitic inductance and to provide filtering function to prevent the switching current from flowing back to the battery rail. A 10µF/6.3V ceramic capacitor (X5R or X7R) is a good starting point for the input capacitor selection.

Output Voltage Setting Resistor Selection

The voltage divider resistors, R_1 and R_2 , (as shown in Figure 19), set the desired output voltage value. The output voltage can be calculated using Equation 2:

$$V_O = V_{FB} \cdot \left(1 + \frac{R_1}{R_2}\right) \quad (\text{EQ. 2})$$

Where V_{FB} is the feedback voltage (typically it is 0.8V). The current flowing through the voltage divider resistors can be calculated as $V_O/(R_1 + R_2)$, so larger resistance is desirable to minimize this current. On the other hand, the FB pin has leakage current that will cause error in the output voltage setting. The leakage current has a typical value of 0.1µA. To minimize the accuracy impact on the output voltage, select the R_2 no larger than 200kΩ.

C3 (shown in Figure 19) is highly recommended to be added for improving stability, and achieving better transient response. C3 should be 120pF or less to meet the 60µs maximum soft-startup time when $STBY = 1$.

Table 1 provides the recommended component values for some output voltage options.

Layout Recommendation

The PCB layout is a very important converter design step to make sure the designed converter works well, especially under the high current high switching frequency condition.

For ISL9109, the power loop is composed of the output inductor L, the output capacitor C_{OUT} , the SW pin and the GND pin. It is necessary to make the power loop as small as possible and the connecting traces among them should be direct, short and wide; the same type of traces should be used to connect the VIN pin, the input capacitor C_{IN} and its ground. The switching node of the converter, the SW pin, and the traces connected to this node are very noisy, so keep the voltage feedback trace and other noise sensitive traces away from these noisy traces.

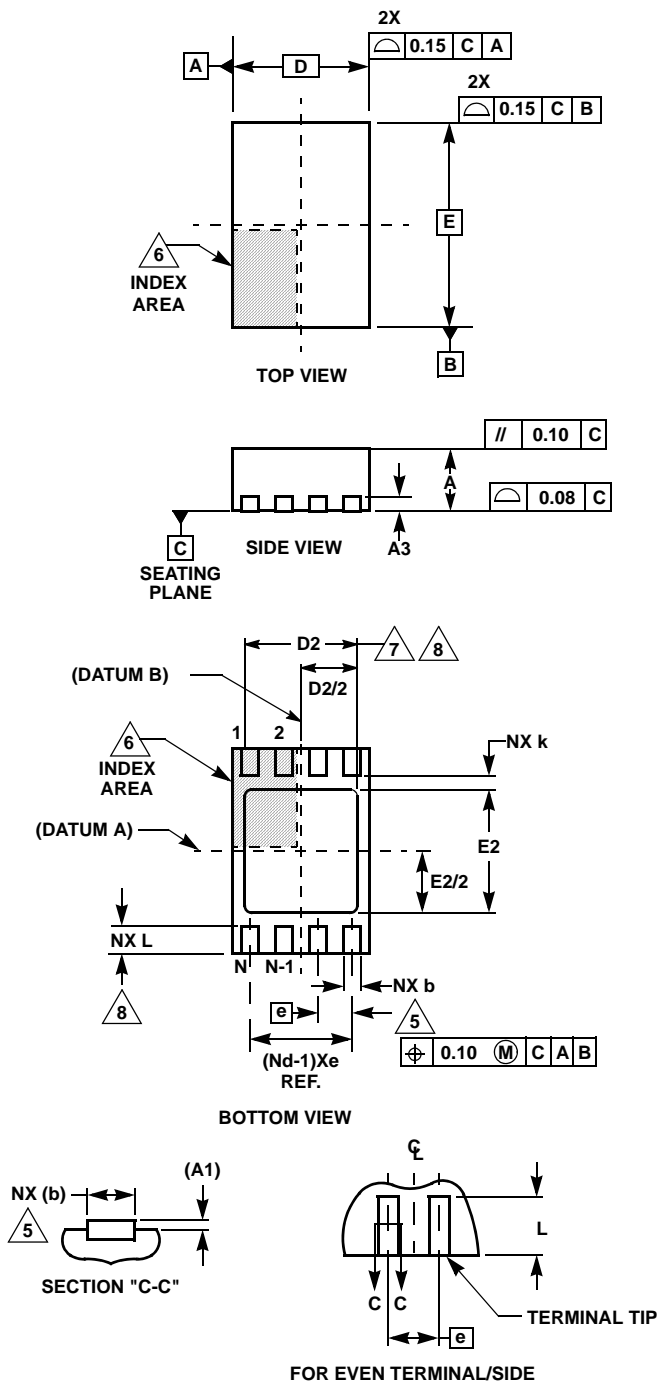
The input capacitor should be placed as close as possible to the VIN pin. The ground of the input and output capacitors should be connected as close as possible as well.

The heat of the IC is mainly dissipated through the thermal pad. Maximizing the copper area connected to the thermal pad is preferable. In addition, a solid ground plane is helpful for EMI performance.

TABLE 1. ISL9109 CIRCUIT CONFIGURATION vs V_{OUT}

VOUT (V)	L (μ H)	C2 (μ F)	R1 ($k\Omega$)	C3 (pF)	R2 ($k\Omega$)
0.8	2.2	10	0	N/A	100
1.0	2.2	10	44.2	120	178
1.2	2.2	10	80.6	120	162
1.5	2.2	10	84.5	100	97.6
1.8	2.2	10	100	100	80.6
2.5	2.2	10	100	100	47.5
2.8	2.2	10	100	100	40.2
3.3	2.2	10	102	100	32.4

Dual Flat No-Lead Plastic Package (DFN)



L8.2x3

8 LEAD DUAL FLAT NO-LEAD PLASTIC PACKAGE

SYMBOL	MILLIMETERS			NOTES
	MIN	NOMINAL	MAX	
A	0.80	0.90	1.00	-
A1	-	-	0.05	-
A3	0.20 REF			-
b	0.20	0.25	0.32	5,8
D	2.00 BSC			-
D2	1.50	1.65	1.75	7,8
E	3.00 BSC			-
E2	1.65	1.80	1.90	7,8
e	0.50 BSC			-
k	0.20	-	-	-
L	0.30	0.40	0.50	8
N	8			2
Nd	4			3

Rev. 0 6/04

NOTES:

1. Dimensioning and tolerancing conform to ASME Y14.5-1994.
2. N is the number of terminals.
3. Nd refers to the number of terminals on D.
4. All dimensions are in millimeters. Angles are in degrees.
5. Dimension b applies to the metallized terminal and is measured between 0.25mm and 0.30mm from the terminal tip.
6. The configuration of the pin #1 identifier is optional, but must be located within the zone indicated. The pin #1 identifier may be either a mold or mark feature.
7. Dimensions D2 and E2 are for the exposed pads which provide improved electrical and thermal performance.
8. Nominal dimensions are provided to assist with PCB Land Pattern Design efforts, see Intersil Technical Brief TB389.

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