

SiGe Wideband direct Quadrature Modulator w/ vGa, 50 - 2800 MHz

HMC795LP5E

typical applications

The HMC795LP5E is ideal for:

- UMTS, GSM or CDMA Basestations
- Fixed Wireless or WLL
- ISM Transceivers, 900 & 2400 MHz
- GMSK, QPSK, QAM, SSB Modulators
- Cellular/3G and WiMAX/4G
- Microwave IFs

Functional Diagram

Features

High Linearity OIP3: + 22 dBm

High Output Power: +10 dBm Output P1dB

High Carrier Suppression: 55 dBc

High Sideband Suppression: 53 dBc

- Read/Write Serial Port Interface (SPI)
- SPI & 6-bit parallel port programmable 32 dB Gain Control
- DC 440 MHz Baseband Input

32 Lead 5x5 mm QFN Package: 25 mm2

General Description

The HMC795LP5E is a variable gain, direct quadrature modulator ideal for digital modulation applications from 50 - 2800 MHz including: Cellular/3G, Broadband Wireless Access and ISM circuits. Housed in a compact 5x5mm (LP5) SMT QFN package, the modulator offers a high level of integration, exceptionally low carrier feedthrough, and a low cost alternative to more complicated double upconversion architectures.

The LO requires -9 to +3 dBm and can be driven in either differential or single-ended mode. The baseband inputs will support modulation inputs from DC - 440 MHz.

The differential RF output port is driven by a 6 bit digital controlled variable gain amplifier to nominally provide up to 32 dB of very linear gain control in 0.5 dB steps. The low carrier suppression is maintained over the VGA dynamic range. The gain control interface accepts either three wire serial input or 6 bit parallel word. In addition, the gain control can be modified through the SPI to adjust a look up table to control the gain step to as low as 0.1 dB, with reduced range, or to adjust individual gain steps for system linearization.

electrical Speciications, See test conditions on Following Page

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Electrical Specifications (Continued)

Test Conditions: Unless Otherwise Specified, the Following Test Conditions Were Used

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Calibrated vs. Uncalibrated Test Results

During the Uncalibrated Carrier Suppression tests, care is taken to ensure that the I/Q signal paths from the Vector Signal Generator (VSG) to the Device Under Test (DUT) are equal. The "Uncalibrated" Carrier Suppression plots were measured at T= -40 $^{\circ}$ C, +25 $^{\circ}$ C, and +85 $^{\circ}$ C.

The "Calibrated" Carrier Suppression data was plotted after a manual adjustment of the IP/IN & QP/QN DC offsets at +25 °C, 5V Vcc, 0 dBm LO input power level, and the RF output frequency set to the midband of the measurement range. The adjustment settings were held constant during tests over temperature and frequency.

typical Performance characteristics, vcc +5v, lo 0 dbm, +25 °c

SIDEBAND SUPPESSION

Output Power & Output Noise @ 1 GHz vs. *VGA Attenuation over Temperature* ^[1]

[1] Output Matched to 1 GHz

uncalibrated & calibrated carrier Feedthrough vs. Freq. over temperature [1]

carrier Feedthrough & Sideband Suppression @ 1 GHz vs. vGa attenuation over temperature [1]

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Output Power & Output Noise @ 1 GHz vs. input baseband amplitude over temperature [1]

output Power, output iP3 & Sideband Suppression vs. Freq. over LO Power^[1]

Output Power, Output IP3 & Sideband Suppression vs. Freq. over Supply voltage [1]

[1] Output Matched to 1 GHz

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carrier Feedthrough & Sideband Suppression @ 1 GHz vs. input baseband amplitude over temperature [1]

ــا 80-
800 -75 800 850 900 950 1000 1050 1100 1150 1200 0 dBm +3 dBm -9 dBm

uncalibrated & calibrated carrier Feedthrough vs. Freq. over Supply voltage [1]

FREQUENCY (MHz)

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output Power, output iP3 & Sideband Suppression vs. Freq. over temperature [1]

Output Power & Output Noise @ 1950 MHz vs. vGa attenuation MHz over temperature [1]

Output Power & Output Noise @ 1950 MHz vs. input baseband amplitude over temperature [1]

uncalibrated & calibrated carrier Feedthrough vs. Freq. over Temperature [1]

carrier Feedthrough & Sideband Suppression @ 1950 MHz vs. vGa attenuation over temperature [1]

carrier Feedthrough & Sideband Suppression @ 1950 MHz vs. input baseband amplitude over temperature [1]

[1] Output Matched to 1950 MHz

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uncalibrated & calibrated carrier

output Power, output iP3 & Sideband Suppression vs. Freq. over LO Power^[1]

output Power, output iP3 & Sideband Suppression vs. Freq. over Supply voltage [1]

output Power, output iP3 & Sideband Suppression vs. Freq. over temperature [2]

uncalibrated & calibrated carrier Feedthrough vs. Freq. over Supply voltage [1]

uncalibrated & calibrated carrier Feedthrough vs. Freq. over temperature [2]

[1] Output Matched to 1950 MHz [2] Output Matched to 2690 MHz

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output Power & output noise @ 2690 MHz vs. vGa attenuation over temperature [1]

Output Power & Output Noise @ 2960 MHz vs. input baseband amplitude over temperature [1]

output Power, output iP3 & Sideband Suppression vs. Freq. over LO Power^[1]

[1] Output Matched to 2960 MHz

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carrier Feedthrough & Sideband Suppression @ 2960 MHz vs. vGa attenuation over temperature [1]

carrier Feedthrough & Sideband Suppression @ 2960 MHz vs. input baseband amplitude over temperature [1]

uncalibrated & calibrated carrier Feedthrough vs. Freq. over LO Power [1]

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output Power, output iP3 & Sideband Suppression vs. Freq. over Supply voltage [1]

normalized attenuation vs. Frequency (only Major States are Shown)

absolute error [2] vs. attenuation State

[1] Output Matched to 2960 MHz

[2] Absolute error - difference between measured and ideal attenuation

uncalibrated & calibrated carrier Feedthrough vs. Freq. over Supply voltage [1] -30

absolute error [2] vs. Frequency (Only Major States are Shown)

^[3] Step error - difference between measured attuation step and ideal step of 0.5 dB

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LO Return Loss vs. Frequency

acPr for W-cdMa @ 2140 MHz vs. output Power for various input levels, vGA Attenuation 0 dB [1]

RF Return Loss vs. Attenuation

RF Return Loss vs. Frequency Offset, vGa attenuation 0 db

acPr for W-cdMa @ 2140 MHz vs. output Power & vGa attenuation for various input levels [1]

[1] W-CDMA (Modulation Set-up for ACPR Mode): The baseband I and Q input signals were generated using "Test Model 1 with 64 channels

-50 ACPR (dBc)

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Absolute Maximum Ratings Truth Table

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Control Voltage Input **Attenuation** AGC5 | AGC4 | AGC3 | AGC2 | AGC1 | AGC1 Low Low Low Low Low Low 0 dB Low Low Low Low Low High 0.5 dB Low Low Low Low High Low 1 dB Low Low Low High Low Low 2 dB Low Low High Low Low Low 4 dB Low High Low Low Low Low 8 dB High | Low | Low | Low | Low | 16 dB High | High | High | High | High | 31.5 dB

Any combination of the above states will provide an increase in the attenuation approximately equal to the sum of the bits selected

ELECTROSTATIC SENSITIVE DEVICE OBSERVE HANDLING PRECAUTIONS

5. PACKAGE WARP SHALL NOT EXCEED 0.05mm.

6. ALL GROUND LEADS AND GROUND PADDLE MUST BE SOLDERED TO PCB RF GROUND.

7. REFER TO HITTITE APPLICATION NOTE FOR SUGGESTED LAND PATTERN.

Package information

[2] Max peak reflow temperature of 260 °C

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Pin Descriptions

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Pin Descriptions (Continued)

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Evaluation PCB

The circuit board used in the application should use RF circuit design techniques. Signal lines should have 50 ohm impedance while the package ground leads and exposed paddle should be connected directly to the ground plane similar to that shown. A sufficient number of via holes should be used to connect the top and bottom ground planes. The evaluation circuit board shown is available from Hittite upon request.

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List of Materials for Evaluation PCB [1]

[1] When requesting an evaluation board, please reference the appropriate PCB number listed in the table "Components for the Selected Frequencies"

[2] Circuit Board Material: Arlon 25FR / FR4

table 9. components for Selected Frequencies

[1] Evaluation Kit includes evaluation board, USB controller board, USB cable and evaluation software.

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Application & Evaluation PCB Schematic

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Theory of Operation

The HMC795LP5E modulator consists of the following functional blocks

- 1. LO Interface
- 2. I/Q modulator
- 3. Digitally controlled variable gain amplifier
- 4. Gain control DAC
- 5. Bias Circuit
- 6. Serial Port interface

lo interface

The LO interface consists of a gain stage followed by a divide by 2 stage that generates two carrier signals in quadrature which are used to drive the mixers. As a result, the LO path is immune to large variations in the LO signal level and the modulator performance does not vary much with LO power. Due to the on chip divider, the input LO frequency must be twice that of the desired carrier frequency. This offers the advantage of significantly lowering carrier feedthrough.

The LO port can be driven differentially or single ended if the unused side is AC grounded. However, when driven single-endedly, the carrier feedthrough and sideband rejection can be degraded by either large 2nd order LO tones, such as when driven by a VCO with a divider output, or, by large half-harmonic tones, such as when driven by a VCO with a doubler output.

The LO interface can be enabled/disabled separately through the serial port interface using Reg01h <0> and can be used to disable the modulator output. The RF output signal is suppressed by 100 dB when only the LO interface is disable and the LO signal itself is suppressed approximately 60 dB. In addition, the LO buffer bias can be increased using Reg02h <7>. This setting is recommended for LO frequencies above 5 GHz.

i/Q Modulator

The HMC795LP5E has two double-balanced mixers, one for the in-phase channel and one for the quadrature channel. The differential baseband inputs (QP, QN, IP, and IN) consist of the bases of NPN transistors, which present a high impedance. The DC common mode voltage at the baseband inputs sets the currents in the two mixer cores. Varying the baseband common mode voltage varies the current in the mixers and affects the overall modulators performance. The recommended DC voltage for the baseband common mode voltage is 1.3V DC, \pm 0.1V.

The output of the two mixers are summed together differentially and then used to drive the differential input of the VGA stage. The mixer can be enabled/disabled with Reg01h <1>. The external baseband DC bias also need to be disabled to completely disable the mixers. Disabling the mixer enables a weak pull down at the mixer inputs which connects the mixer inputs through a resistive path to ground. This may pull the external input low resulting in large current low if the external bias is not disabled.

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Digitally Controlled Variable Gain Amplifier

The output of the HMC795LP5E is a 6 bit, digitally controlled, variable gain amplifier that can provide very accurate linear- in-dB gain control over a 31.5 dB range in 0.5 dB steps. The VGA also provides relatively constant phase over the entire gain range, as shown in Figure 1. An 11 bit DAC is used to control the VGA. See the Gain Control DAC section for more detail about gain control.

Figure 1. VGA S21 magnitude and phase @ 2 GHz vs attenuation

For maximum performance and lexibility, the output ports of the VGA are differential open collectors that require pull up inductors to the positive supply and external matching components. The evaluation board allows for several options for matching. See the Output Matching section for more details.

The VGA can be enabled/disabled separately through the SPI using Reg01h <2>. The ON/OFF isolation of the VGA is greater than 60 dB for RF output frequencies up to 2.5 GHz.

Gain Control DAC

An 11 bit DAC is used to control the VGA for linear-in-dB gain control, Figure 2 shows the control for the DAC.. The DAC is normally controlled by a look up table (LUT) that is in turn, controlled by the 6 bit parallel port. The values of the look up table are ixed to give 0.5 dB steps over a 31.5 dB gain range.

Figure 2. Simpliied DAC control diagram

For increased flexibility, there are three methods to control the DAC and VGA gain.

1. **Parallel Mode** Use the 6 bit parallel port to provide ixed 0.5 dB gain steps. In this mode the DAC is controlled by a look up table with 64 states that map the 6 bit parallel port to ixed 11-Bit gain words for each state. The values of the LUT are fixed to give nominally 0.5 dB attenuation steps over a 31.5 dB gain range.

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2. **Correction Mode** Use the SPI port in conjunction with the 6 bit parallel port to apply a 4 bit, 2's complement, correction factor to any attenuation step. This option can be used to compensate the gain control for systematic variations in the transmit chain by adding negative or positive correction factors to any of the ixed LUT values to either slightly increase or decrease the gain step for that particulate state. This mode requires the host controller to write the desired corrections to the SPI after the chip is powered up. The correction factors are then applied to the desired gain steps when ever the parallel port gain control changes, until the chip is powered down.

 The 4 bit, 2's compliment, correction factor for each line in the LUT are set by Reg4h to Reg13h. The correction factor for 0 dB attenuation (line 0) is set in Reg4h <3:0>, 0.5 dB (line 1) is set by Reg4h <7:4>, 1.0 dB (line 2) by Reg4h<11:8> and so on until Reg13h <15:12> which sets the correction factor for 31.5 dB attenuation. If more adjustment is needed, the LUT correction values can be increased by a factor of 2, 3, or 4 times by using Reg2h <15:8>. Reg2h <9:8> sets the multiplication factor for the irst quadrant of the LUT, lines 0 to 15, <11:10> for lines 16 to 31, <13:12> for lines 32 to 47 and <15:14> for the last quadrant, lines 48 to 63. The correction in dB can be estimated by

$$
COR(dB) = 10 \cdot log10 \left[\left(1 + \frac{(CORword \cdot mult)}{LUTword} \right)^{-1} \right]
$$

where mult is the correction multiplication factor, and CORword and LUTword are the decimal equivalent of the binary correction and LUT word. An expression for determining the LUTword is given in the bypass mode section below. Figures 3, 4 and 5 show the range of correction in dB for 4 dB, 16 dB and 31.5 dB attenuation and Figure 6 shows the output power versus attenuation for no correction, maximum positive and maximum negative correction applied to all states in the LUT. The LUT value for 0 dB attenuation can only be decreased since it already at maximum. Increasing the word value will cause an overlow resulting in maximum attenuation instead.

Figure 3. Attenuation Change from 4 dB Attenuation vs. LUT Correction Word over Different Multiplication Factors

Figure 4. Attenuation Change from 16 dB Attenuation vs. LUT Correction Word over Different Multiplication Factors

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Figure 5. Attenuation Change from 31.5 dB Attenuation vs. LUT Correction Word over Different Multiplication Factors

Figure 6. Output Power @ 850 MHz vs. VGA Attenuation for no Correction, Maximum Positive & Maximum Negative Correction Values

3. **Bypass Mode**. Use the SPI port to bypass the parallel port and LUT completely. In this mode Reg2h<4> is set to enable the bypass mode. The host controller can then write the desired gain word to the SPI using Reg3h<10:0> for each and every desired gain change. The input word can be determined from the desired gain (in dB) by

 $LUTword(10:0) = dec2bin[round(2^{11} - 1) \cdot 10^{(-attn)/20}]$

 and is plotted in Figure 7. In the this mode it is possible to use much lower attenuation steps over a reduced gain control range. The limit for reliable attenuation steps is 0.1 dB with a gain control range of approximately 22 dB.

Figure 7. Attenuation vs. LUT word

The DAC can be enabled/disabled separately through the serial port interface using bit 3 of register 01h. Disabling the DAC will also disable the VGA.

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bias circuit

A band gap reference circuit generates the reference currents used by the different sections. The bias circuit can be disabled with Reg01h <4>. Disabling the bias circuit will also disable the reference currents to all the other sections except the mixers, since they use an external bias. An external pin, pin 24, is also provided to allow for external decoupling for low noise performance, 100nF is recommended.

Power on Reset and Soft Reset

The HMC795LP5E features a hardware Power On Reset (POR). All chip registers will be reset to default states approximately 250 us after power up. The SPI registers may also be hardware reset by holding RSTB, pin 1, low, or software reset by writing 80h to Reg00h followed by writing 00h to Reg00h.

Serial Port interface

The HMC795LP5E features a four wire serial port for simple communication with the host controller. Register types may be Read Only, Write Only, or Read/Write, as described in the registers descriptions. Typical serial port operation can be run with SCK at speeds up to 50 MHz. The HMC795LP5E chip address is ixed as "4d" or "100b".

Serial Port WRITE Operation

A typical WRITE cycle is shown in Figure 8. It is 40 clock cycles long.

- 1. The host both asserts SEN (active low Serial Port Enable) and places the MSB of the data on SDI followed by a rising edge on SCLK.
- 2. HMC795LP5E reads SDI on the 1st rising edge of SCLK after SEN.
- 3. HMC795LP5E registers the data bits in the next 29 rising edges of SCLK.
- 4. Host places the seven register address bits on the next seven falling edges of SCLK, MSB irst.
- 5. HMC795LP5E registers the register address bits in the next seven rising edges of SCLK.
- 6. Host places the 3 chip address bits <100> on the next 3 falling edges of SCLK, MSB irst.
- 7. HMC795LP5E registers the chip address bits in the next 3 rising edges of SCLK.
- 8. SEN is de-asserted on the 40th falling edge of SCLK. This completes the WRITE cycle.
- 9. HMC795LP5E also exports data back on the SDO line. For details see the section on READ operation.

The host changes the data on the falling edge of SCLK and the HMC795LP5E reads the data on the rising edge.

Serial Port READ Operation

The SPI can read from the internal registers in the chip. The data is available on SDO line. This line itself is tri-stated after power up. After a WRITE cycle, the HMC795LP5E controls the SDO line and exports data on this line during the current WRITE cycle. The HMC795LP5E chip address is fixed as '4d' or '100b'

A READ operation is always preceded by a WRITE operation to Register 0 to deine the register to be queried. Every READ cycle is also a WRITE cycle in that data sent to the SPI while reading the data will also be stored by the HMC795LP5E when SEN goes high. If this is not desired then it is suggested to write to Register 0 during the READ operation as the status of the device will be unaffected.

A typical READ cycle is also shown in Figure 8. A read cycle is 40 clock cycles long. To specifically read a register, the address of that register must be written in the register 0. A read cycle can then be initiated as follows;

- 1. The host asserts SEN (active low Serial Port Enable) followed by a rising edge SCLK.
- 2. HMC795LP5E reads SDI (the MSB) on the 1st rising edge of SCK after SEN.

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- 3. HMC795LP5E registers the data bits in the next 29 rising edges of SCLK (total of 30 data bits). The LSBs of the data bits represent the address of the register that is intended to be read.
- 4. Host places the 7 register address bits on the next 7 falling edges of SCLK (MSB to LSB) while the HMC795LP5E reads the address bits on the corresponding rising edge of SCK. For a read operation this is "0000000".
- 5. Host places the 3 chip address bits <100> on the next 3 falling edges of SCK (MSB to LSB). Note

the HMC795LP5E chip address is fixed as "4d" or "100b".

- 6. SEN goes from low to high after the 40th rising edge of SCK. This completes the irst portion of the READ cycle.
- 7. The host asserts SEN (active low Serial Port Enable) followed by a rising edge SCLK.
- 8. HMC795LP5E places the 30 data bits, 7 address bits, and 3 chip id bits on the SDO on each rising edge of the SCK commencing with the first rising edge beginning with MSB.
- 9. The host de-asserts SEN (i.e. sets SEN high) after reading the 40 bits from the SDO output. The 32 bits consists of 30 data bits, 7 address bits, and the 3 chip id bits. This completes the READ cycle.

Figure 8. SPI Timing Diagram for write and read operation

Main SPI Timing Characteristics $DVDD = +3.3V \pm 10\%$, GND = 0V

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output Matching

The output ports of the VGA are differential open collectors that require pull up inductors to the positive supply and external matching components. The evaluation board uses a 2:1 impedance transformer to convert the differential output to single ended for evaluation purposes. Three options are available for the evaluation board, each with different matching components, one for 850 MHz, one for 1950 MHz, and another for 2690 MHz. When requesting an evaluation board, please reference the appropriate PCB number listed in the table "Components for the Selected Frequencies"

There are a number of ways to match the RF output of the HMC795LP5E for optimum performance. The most basic method is to use a 50 Ω resistor to Vcc and a 1 nF dc bypass capacitor connected in series as shown Figure 9(a). This option provides a good broadband match, see Figure 10, but limits the maximum output power, compared to a narrow band match, see Figure 11. Single-ended operation is possible by using a transformer, which can limit the bandwidth, as seen in the output power plot, or by using only one side of the differential output. However, biasing for the unused side is still required. For best performance it is recommended to terminate the unused side with the same matching and load impedance as the used side, see Figure 9(b). Output power is generally reduced by 2 to 3 dB for singleended operation, as shown in Figure 11.

Figure 9. Simple output matching network

[2] With TCN2-26 Transformer

A narrow band solution, with higher output power, is possible by using a simple L-match network, as shown in Figure 12. A shunt resistor is included to control the Q of the matching network and sets the output power of the HMC795LP5E. Consequently a low value resistor will result in a broadband match but lower output power than a high value resistor. The table below provides recommend component values for various output frequencies with a bandwidth of approximately 5-10%. It is also possible to use an LC matching network where L2 is removed and the DC blocking capacitor is used as a matching component. Experiments show that the output power is reduced approximately 1 -2 dB though and that values for the capacitors become unrealistic (< 500 fF) above 2 GHz.

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Figure 12. Simple output matching network

recommending Matching components

DAC Modulator Interface Network

The HMC795LP5Eis capable of interfacing with a variety of popular D/A Convertors. Most DAC have differential outputs with a source or sink current of 0 mA to 20 mA. However, most DACs require a different output compliance voltage than that of the DC input bias level for the HMC795LP5E. A passive interface network can be used to transform the common-mode voltage of the DAC to the desired DC input bias of the modulator of 1.3V. Figures 13 and 14 show the interface network for two different topologies.

- 1. Topology 1. DAC Vcm > HMC795LP5E Vcm. This topology is used shift the DAC output common mode voltage down to the required DC level at the modulator input.
- 2. Topology 2. DAC Vcm < HMC795LP5E Vcm. This topology is used shift the DAC output common mode voltage up to the required DC level at the modulator input.

The resistive level-shifting network is not frequency sensitive but the resistive divider network inherent in the network attenuates the baseband signal. The bypass capacitors shown Figures 13 and 14 will eliminate the attenuation for frequencies greater than 3 kHz. Either topology can be used on the HMC795LP5E evaluation board.

Figure 13. DAC Interface network topology 1

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Figure 14. DAC Interface network topology 2

DAC Interface Network Values

Register Map

Reg 01h - Enable / Control Register

Reg 02h - Function Register

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Reg 02h - Function Register

(E)

reg 03h - Gain control

Reg 04h - LUT Correction 0 - 3

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 0 -15 (attenuation 0 to 7.5 dB) is set in Reg2 by bits mult_0 [9:8]

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Reg 05h - LUT Correction 4 - 7

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 0 -15 (attenuation 0 to 7.5 dB) is set in Reg2 by bits mult_0 [9:8]

Reg 06h - LUT Correction 8 - 11

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 0 -15 (attenuation 0 to 7.5 dB) is set in Reg2 by bits mult_0 [9:8]

Reg 07h - LUT Correction 12 - 15

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 0 -15 (attenuation 0 to 7.5 dB) is set in Reg2 by bits mult_0 [9:8]

Reg 08h - LUT Correction 16 - 19

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 16 - 31 (attenuation 8 to 15.5 dB) is set in Reg2 by bits mult_0 [11:10]

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reg 09h - lut correction 20 - 23

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 16 - 31 (attenuation 8 to 15.5 dB) is set in Reg2 by bits mult_0 [11:10]

Reg 0Ah - LUT Correction 24 - 27

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 16 - 31 (attenuation 8 to 15.5 dB) is set in Reg2 by bits mult_0 [11:10]

Reg 0Bh - LUT Correction 28 - 31

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 16 - 31 (attenuation 8 to 15.5 dB) is set in Reg2 by bits mult_0 [11:10]

Reg 0Ch - LUT Correction 32 - 35

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 32 - 47 (attenuation 15 to 23.5 dB) is set in Reg2 by bits mult_0 [13:12]

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Reg 0Dh - LUT Correction 36 - 39

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 32 - 47 (attenuation 15 to 23.5 dB) is set in Reg2 by bits mult_0 [13:12]

Reg 0Eh - LUT Correction 40 - 43

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 32 - 47 (attenuation 15 to 23.5 dB) is set in Reg2 by bits mult_0 [13:12]

Reg 0Fh - LUT Correction 44 - 47

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 32 - 47 (attenuation 15 to 23.5 dB) is set in Reg2 by bits mult_0 [13:12]

Reg 10h - LUT Correction 48 - 51

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 48 - 63 (attenuation 24 to 31.5 dB) is set in Reg2 by bits mult_0 [15:14]

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Reg 11h - LUT Correction 52 - 55

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 48 - 63 (attenuation 24 to 31.5 dB) is set in Reg2 by bits mult_0 [15:14]

Reg 12h - LUT Correction 56 - 59

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 48 - 63 (attenuation 24 to 31.5 dB) is set in Reg2 by bits mult_0 [15:14]

reg 13h - lut correction 60 - 63

LUT correction values below can also be multiplied by 1,2,3, or 4 if more correction is needed. Multiplication factor for LUT lines 48 - 63 (attenuation 24 to 31.5 dB) is set in Reg2 by bits mult_0 [15:14]

SiGe WIDEBAND DIRECT QUADRATURE Modulator w/ vGa, 50 - 2800 MHz

characterization Set-up

