**10 Channel LED Backlight Driver with Integrated Power Supply**

The 34844/A is a high efficiency, LED driver for use in backlighting LCD displays from 10" to 20"+. Operating from supplies of 7.0 to 28 V, the MC34844/A is capable of driving up to 160 LEDs in 10 parallel strings. Current in the 10 strings is matched to within ±2%, and can be programmed via the I<sup>2</sup>C/SM Bus interface.

The 34844/A also includes a Pulse Width Monitor (PWM) generator for LED dimming. The LEDs can be dimmed to one of 256 levels, programmed through the I<sup>2</sup>C/SM Bus interface. Up to 65,000:1 (256:1 PWM, 256:1 Current DAC) dimming ratio.

The integrated boost converter generates the minimum output voltage required to keep all LEDs illuminated with the selected current, providing the highest efficiency possible.

The 34844 has an integrated boost self-clocks at a default frequency of 600 kHz, but may be programmed via  $I^2C$  to 150/300/ 600/1200 kHz. The PWM frequency can be set from 100 Hz to 25 kHz, or can be synchronized to an external input. If not synchronized to another source, the internal PWM rate outputs on the CK pin. This enables multiple devices to be synchronized together.

The 34844A has a default boost frequency of 320 kHz, but may be programmed via I<sup>2</sup>C to 160/320/650/1300 kHz. The PWM frequency can be set from 110 Hz to 27 kHz, or can be synchronized to an external input. If not synchronized to another source, the internal PWM rate outputs on the CK pin. This enables multiple devices to be synchronized together.

The 34844/A also supports optical/temperature closed loop operation and also features LED over-temperature protection, LED short protection, and LED open circuit protection. The IC also includes over-voltage protection, over-current protection, and under-voltage lockout.

#### **Features**

- Input voltage of 7.0 to 28 V
- 2.5 A integrated boost FET
- Up to 50 mA on the 34844 LED current per channel
- Up to 80 mA on the 34844A LED current per channel
- 90% efficiency (DC:DC)
- $\cdot$  I<sup>2</sup>C/SM Bus interface
- 10 channel current mirror with ±2% current matching
- Boost output voltage up to 60V, with Dynamic Headroom Control (DHC)
- PWM frequency programmable or synchronizable from 100 to 25,000 Hz for the 34844
- PWM frequency programmable or synchronizable from 110 to 27,000 Hz for the 34844A
- 32-Ld 5x5x1.0mm TQFN Package

### **Applications**

- Monitors and HDTV up to 42 inch
- Personal Computer Notebooks
- **GPS Screens**
- Small screen Televisions

\* This document contains certain information on a new product. Specifications and information herein are subject to change without notice. © Freescale Semiconductor, Inc., 2009-2012. All rights reserved.



Document Number: MC34844 Rev. 9.0, 3/2012

**VROHS** 

**34844 34844A**

### **LED DRIVER**



**EP SUFFIX (PB-FREE) 98ASA10800D 32-PIN QFN-EP**

#### **ORDERING INFORMATION**





 **Figure 1. MC34844 Simplified Application Diagram (SM Bus Mode)**



 **Figure 2. MC34844A Simplified Application Diagram (Manual Mode)**

# **DEVICE VARIATIONS**

MC34844 is within the [MC34844 Specifications Pages 4 to 31](#page-3-0), MC34844A is within the [MC34844A Specifications Pages 32](#page-31-0)  [to 54](#page-31-0)

**Table 1. Key Device Variations between the MC34844 and MC34844A**

Electrical Parameter <sup>(1)</sup>	Condition	Value	Unit
Maximum LED Current			m <sub>A</sub>
34844		55	
34844A		85	
<b>LED Channel Sink Current</b>		(typ)	mA
34844	RISET=5.1 kQ +0.1%	50	
34844A	RISET=3.48 k $\Omega$ +0.1%	80	
Switching Frequency		(typ)	MHz
34844	$(BST [1:0]=0)$	0.15	
	$(BST [1:0]=1)$	0.30	
	(BST [1:0]=2) [default]	0.60	
	$(BST [1:0]=3)$	1.20	
34844A	$(BST [1:0]=0)$	0.16	
	(BST [1:0]=1)) [default]	0.32	
	$(BST [1:0]=2)$	0.65	
	$(BST [1:0]=3)$	1.30	
<b>PWM Frequency Range</b>	This frequency range applies for Master		Hz
34844	mode, Slave mode, and Manual mode	100 - 25000	
34844A		110 - 27000	

<span id="page-2-0"></span>Notes

1. Refer to the respective Electrical Parameters for specific details

# <span id="page-3-0"></span>**MC34844 SPECIFICATIONS PAGES 4 TO 31**

**34844**

 $\Gamma$  $\daleth$ **SWA** VIN<sup>-</sup> □ SWB VDC1 $\Gamma$ LDO  $\Box$  A0/SEN VDC<sub>2</sub>  $\overline{\phantom{a}}$ OVP VDC3 PGNDA COMP<sup>[</sup> BOOST **PGNDB** CONTROLLER SLOPE<sup><sup>+</sup></sup> VOUT  $\square$  $CK$ V SENSE  $\Box$  FAIL CLOCK/PLL EN M/~S $\overline{\phantom{0}}$  IO PWM GENERATOR PWM ור'  $\Box$  I2 SCK  $\Box$ I3 10 CHANNEL SDA 50 mA CURRENT | 14 MIRROR I <sup>2</sup>C INTERFACE  $\Box$ I5  $\overline{\phantom{0}}$  16  $\Box$  17  $\Box$ I8  $\Box$  I9 **ISET** CURRENT DAC  $\overline{\phantom{a}}$ PIN  $\mathbf{L}$ TEMP/OPTO  $\overline{\phantom{a}}$  GND OCP/OTP/UVLO LOOP CONTROL NIN  $\Box$  $\Box$ 

**INTERNAL BLOCK DIAGRAM**

 **Figure 3. 34844 Simplified Internal Block Diagram**

Analog Integrated Circuit Device Data 5 Freescale Semiconductor



## **PIN CONNECTIONS**



 **Figure 4. 34844 Pin Connections**

# **Table 2. 34844 Pin Definitions**

A functional description of each pin can be found in the Functional Pin Description section beginning on [page](#page-13-0) 14.



**34844**

### **Table 2. 34844 Pin Definitions (continued)**

A functional description of each pin can be found in the Functional Pin Description section beginning on page 14.



# **ELECTRICAL CHARACTERISTICS**

### *MAXIMUM RATINGS*

#### **Table 3. Maximum Ratings**

All voltages are with respect to ground, unless otherwise noted. Exceeding these ratings may cause a malfunction or permanent damage to the device.



Notes

<span id="page-7-1"></span>2. ESD testing is performed in accordance with the Human Body Model (HBM) (AEC-Q100-2), and the Machine Model (MM) (AEC-Q100- 003),  $R_{ZAP}$  = 0  $\Omega$ 

<span id="page-7-2"></span>3. Per JEDEC51 Standard for Multilayer PCB

<span id="page-7-3"></span>4. Pin soldering temperature limit is for 10 seconds maximum duration. Not designed for immersion soldering. Exceeding these limits may cause malfunction or permanent damage to the device.

<span id="page-7-0"></span>5. 45 V is the Maximum allowable voltage on all LED channels in off-state.

## *STATIC AND DYNAMIC ELECTRICAL CHARACTERISTICS*

#### **Table 4. Static and Dynamic Electrical Characteristics**

Characteristics noted under conditions V<sub>IN</sub> = 12 V, V<sub>OUT</sub> = 42 V, I<sub>LED</sub> = 50 mA, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1, -40 °C  $\leq$  T<sub>A</sub> $\leq$  105 °C, PGND = 0 V, unless otherwise noted.





<span id="page-8-0"></span>Notes

6. This output is for internal use only and not to be used for other purposes. A 1.0 kΩ resistor between the VDC3 and VDC1 pin is recommended for <-20 °C operation.

<span id="page-8-2"></span><span id="page-8-1"></span>7. Minimum and Maximum output voltages are dependent on Min/Max duty cycle condition.

### **Table 4. Static and Dynamic Electrical Characteristics (continued)**

Characteristics noted under conditions V<sub>IN</sub> = 12 V, V<sub>OUT</sub> = 42 V, I<sub>LED</sub> = 50 mA, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1, -40 °C  $\leq$  T<sub>A</sub> $\leq$  105 °C, PGND = 0 V, unless otherwise noted.



47.50

50

52.50

<span id="page-9-0"></span>Notes

 $PIN = V_{SET}$ 

#### ELECTRICAL CHARACTERISTICS *STATIC AND DYNAMIC ELECTRICAL CHARACTERISTICS*

### **Table 4. Static and Dynamic Electrical Characteristics (continued)**

Characteristics noted under conditions V<sub>IN</sub> = 12 V, V<sub>OUT</sub> = 42 V, I<sub>LED</sub> = 50 mA, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1, -40 °C  $\leq$  T<sub>A</sub>  $\leq$  105 °C, PGND = 0 V, unless otherwise noted.



<span id="page-10-0"></span>Notes

### **Table 4. Static and Dynamic Electrical Characteristics (continued)**

Characteristics noted under conditions V<sub>IN</sub> = 12 V, V<sub>OUT</sub> = 42 V, I<sub>LED</sub> = 50 mA, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1, -40 °C  $\leq$  T<sub>A</sub> $\leq$  105 °C, PGND = 0 V, unless otherwise noted.



Notes

#### ELECTRICAL CHARACTERISTICS *STATIC AND DYNAMIC ELECTRICAL CHARACTERISTICS*

#### **Table 4. Static and Dynamic Electrical Characteristics (continued)**

Characteristics noted under conditions V<sub>IN</sub> = 12 V, V<sub>OUT</sub> = 42 V, I<sub>LED</sub> = 50 mA, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1, -40 °C  $\leq$  T<sub>A</sub>  $\leq$  105 °C, PGND = 0 V, unless otherwise noted.



<span id="page-12-1"></span>12. Special considerations should be made for frequencies between 100 Hz to 1.0 KHz. Please refer to [Functional Device Operation](#page-20-0) for further details.

<span id="page-12-0"></span>13. Guaranteed by design

**34844**

# **FUNCTIONAL DESCRIPTION**

### *INTRODUCTION*

LED backlighting has become very popular for small and medium LCDs, due to some advantages over other backlighting schemes, such as the widely used cold cathode fluorescent lamp (CCFL). The advantages of LED backlighting are low cost, long life, immunity to vibration, low operational voltage, and precise control over its intensity.

However, there is an important drawback of this method. It requires more power than most of the other methods, and this is a major problem if the LCD size is large enough.

To address the power consumption problem, solid state optoelectronics technologies are evolving to create brighter LEDs with lower power consumption. These new technologies together with highly efficient power management LED drivers are turning LEDs, a more suitable solution for backlighting almost any size of LCD panel, with really conservative power consumption.

One of the most common schemes for backlighting with LED is the one known as "Array backlighting". This creates a matrix of LEDs all over the LCD surface, using defraction and diffused layers to produce an homogenous and even light at the LCD surface. Each row or column is formed by a number of LEDs in series, forcing a single current to flow through all LEDs in each string.

Using a current control driver, per row or column, helps the system to maintain a constant current flowing through each line, keeping a steady amount of light even with the presence of line or load variations. They can also be use as a light intensity control by increasing or decreasing the amount of current flowing through each LED string.

To achieve enough voltage to drive a number of LEDs in series, a boost converter is implemented, to produce a higher voltage from a smaller one, which is typically used by the logical blocks to do their function.

The 34844 implements a single channel boost converter together with 10 input channels, for driving up to 16 LEDs per string to create a matrix of more than 160 LEDs. Together with its 90% efficiency and  $1<sup>2</sup>C$  programmable or external current control, among other features, makes the 34844 a perfect solution for backlighting small and medium size LCD panels, on low power portable and high definition devices.

### *FUNCTIONAL PIN DESCRIPTION*

### <span id="page-13-0"></span>**INPUT VOLTAGE SUPPLY (VIN)**

IC Power input supply voltage, is used internally to produce internal voltage regulation (VDC1, VDC3) for logic functioning, and also as an input voltage for the boost regulator.

## **INTERNAL VOLTAGE REGULATOR 1 (VDC1)**

This pin is for internal use only, and not to be used for other purposes. A capacitor of 2.2 μF should be connected between this pin and ground for decoupling purposes.

### **INTERNAL VOLTAGE REGULATOR 2 (VDC2)**

This pin is for internal use only, and not to be used for other purposes. A capacitor of 2.2  $\mu$ F should be connected between this pin and ground for decoupling purposes.

### **INTERNAL VOLTAGE REGULATOR 3 (VDC3)**

This pin is for internal use only, and not to be used for other purposes. A capacitor of 2.2 μF should be connected between this pin and ground for decoupling purposes. A 1.0 kΩ resistor between the VDC3 and VDC1 pin is recommended for <-20 °C operation.

### **BOOST COMPENSATION PIN (COMP)**

Passive pin used to compensate the boost converter. Add a capacitor and a resistor in series to GND to stabilize the system.

### **IC ENABLE (EN)**

The active high enable pin is internally pulled high through pull-up resistors. Applying 0 V to this pin would stop the IC from working.

### **INPUT/OUTPUT CLOCK SIGNAL (CK)**

This pin can be used as an output clock signal (master mode), or input clock signal (slave mode), to synchronize more than one device.

### **MASTER/SLAVE MODE SELECTION (M/~S)**

Setting this pin High puts the device into Master mode, producing an output synchronization clock at the CK pin. Setting this pin low, puts the device in Slave mode, using the CK pin as an input clock.

#### **EXTERNAL PWM INPUT (PWM)**

This pin is internally pulled down. An external PWM signal can be applied to modulate the LED channel directly in absence of an  $I^2C$  interface.

## **CLOCK I2C SIGNAL (SCK)**

Clock line for I<sup>2</sup>C communication.

## **ADDRESS I2C SIGNAL (SDA)**

Address line for I<sup>2</sup>C communication.

#### **A0/SEN**

Address select, device select pin, or Hardware Overvoltage Protection (OVP) Control.

### **CURRENT SET (ISET)**

Each LED string can drive up to 50 mA. The maximum current can be set by using a resistor from this pin to GND.

### **POSITIVE CURRENT SCALING (PIN)**

Positive current scaling factor for the external analog current control. Applying 0 V to this pin, scales the current to near 0%, and in the same way, applying 2.048 V (Vset), the scale factor is 100%. By applying a voltage higher than 2.2 V, the scaling factor is disabled, and the internal pull-ups are activated.

If PIN pin and NIN pin are used at the same time then by applying 0 V to the PIN pin and 2.048 V to NIN pin, scales the current to near 0%, and in the same way, applying 2.048 V to the PIN pin and 0 V to NIN pin, scales the current to 100%. By applying a voltage higher than 2.2 V, the scaling factor is disabled and the internal pull-ups are activated in both pins.

### **NEGATIVE CURRENT SCALING (NIN)**

Negative current scaling factor for the external analog current control. Setting 0 V to this pin scales the current to 100%, in the same way, setting 2.048 V (Vset) the scale factor is near 0%. By applying a voltage higher than 2.2 V, the scaling factor is disabled and the internal pull-ups are activated.

If PIN pin and NIN pin are used at the same time then by applying 0 V to the PIN pin and 2.048 V to NIN pin, scales the current near 0%, and in the same way, applying 2.048 V to the PIN pin and 0 V to NIN pin, scales the current to 100%.

By applying a voltage higher than 2.2 V, the scaling factor is disabled and the internal pull-ups are activated in both pins.

#### **GROUND (GND)**

Ground Reference for all internal circuits other than the Boost FET.

The Exposed Pad (EP) should be used for thermal heat dissipation.

#### **I0-I9**

Current LED driver, each line has the capability of driving up to 50 mA.

#### **FAULT DETECTION PIN (FAIL)**

When a fault situation is detected, this pin goes into high impedance.

#### **BOOST SLOPE COMPENSATION SETTING RESISTOR (SLOPE)**

Use an external resistor of about 68 kΩ to configure the Boost compensation slope.

#### **POWER GROUND PINS (PGNDA, PGNDB)**

Ground pin for the internal Boost FET.

### **OUTPUT VOLTAGE SENSE PIN (VOUT)**

Input pin to monitor the output voltage. It also supplies the input voltage for the internal regulator 2 (VDC2).

#### **SWITCHING NODE PINS (SWA, SWB)**

Switching node of boost converter.



## *FUNCTIONAL INTERNAL BLOCK DESCRIPTION*



### **REGULATORS/ POWER DOWN**

The 34844 is designed to operate from input voltages in the 7.0 to 28 V range. This is stepped down internally by LDOs to 2.5 V (VDC1 and VDC3) and 6 V (VDC3) for powering internal circuitry. If the input voltage falls below the UVLO threshold, the device automatically enters in power down mode.

#### **Operating Modes:**

The device can be operated by the EN pin and/or SDA/ SCK bus lines, resulting in three distinct operation modes:

- Manual mode, there is no  $I^2C$  capability, the bus line pins must be tied low, and the EN pin controls the ON/OFF operation.
- SM Bus mode, EN pin must be tied low and the device is turned ON by any activity on the bus lines. The part shuts down if the bus lines are held low for more than 27 ms, the 27 ms watchdog timer can be disabled by  $I^2C$  (setting SETI2C bit high) or tying the EN pin high. In Sleep mode (EN bit=0) the device reduces the power consumption by leaving "alive" only the blocks required for  $I^2C$ communication.
- $I<sup>2</sup>C$  mode, has to be configured by  $I<sup>2</sup>C$  communication (SETI2C bit = 1) right after the IC is turned ON, it prevents the part from being turned ON/OFF by the bus. Sleep mode is also present and it is intended to save power, but still keep the IC prepared to communicate by  $I^2C$ . Turning the EN pin OFF, the chip enters into a low power mode.

Mode	<b>EN Pin</b>	<b>SCK/SDA Pins</b>	<sup>2</sup> C Bit Command	<b>Current Consumption</b> <b>Mode</b>	<b>Comments</b>
Manual	Low	Low	N/A	Shutdown	
	High	Low	N/A	Operational	
SM Bus	Low	Low $(> 27$ ms)	$EN bit = X$	Shutdown	
	Low	Active	$EN bit = 0$	Sleep	
	Low	Active	$EN bit = 1$	Operational	
$I^2C$	Low	X	SETI2C bit = $1$	$I2C$ Low Power (Shutdown)	Part Doesn't Wake-up
			CLRI2C bit = $0$		
			$EN bit = X$		
	High	X	SETI2C bit = $1$	Sleep	
			CLRI2C bit = $0$		
			$EN bit = 0$		
	High	X	SETI2C bit = $1$	Operational	
			CLRI2C bit = $0$		
			$EN bit = 1$		

<span id="page-16-0"></span>**Table 5. Operation Current Consumption Modes**

#### **BOOST**

The integrated boost converter operates in nonsynchronous mode and integrates a 2.5 A FET. An integrated sense circuit is used to sense the voltage at the LED current mirror inputs and automatically sets the boost output voltage (DHC) to the minimum voltage needed to keep all LEDs biased with the required current. The DHC is designed to operate under specific pulse width conditions in the LED drivers. It operates for pulse widths higher than 4.0 μs

If the pulse widths are shorter than specified, the DHC circuit will not operate and the voltage across the LED drivers will increase to a value given by the OVP minus the total LED voltage in the LED string. Therefore it is imperative to select the proper OVP level to minimize power dissipation.

The OVP can be set from 11 to 62 V,  $~1$ ,  $~0$  V spaced, using the  $I^2C$  interface (OVP Register). If  $I^2C$  capability is not present, the OVP can be controlled by a resistor divider connected from VOUT to GND with its mid point tied to A0/ SEN pin (threshold =  $6.5$  V). During an OVP condition, the output voltage will go to the OVP level which is programmed via the I2C interface or settled by a resistor divider on A0/SEN pin, or by a zener diode. The formulas to calculate the hardware OVP using any of the two methods are as follows:



#### **HARDWARE OVP**:

The OVP value should be set to greater than the maximum LED voltage over the whole temperature range. A good practice is to set it 5.0 V or so above the max LED voltage.

The boost converter also features internal Over-current Protection (OCP) and has a user programmable Overvoltage Protection (OVP).

The OCP operates on a cycle by cycle basis. However, if the OCP condition remains for more than 10 ms then the device turns off the LED Drivers, the Boost goes to Sleep mode and the output FAULT pin goes into high-impedance. The device can only be restarted by recycling the enable or creating a Power On Reset (POR).

The user can program the boost frequency by  $I^2C$ (BST[1:0]) only after the IC is powered up and before the boost circuit is turned ON for the first time (PWM pin low to high). This sequence avoids boost frequency to be changed inadvertently during operation. The first I<sup>2</sup>C command has to wait for 5.0 ms after the part is turned ON, in order to allow sufficient time for the device power up sequence to be completed.

The boost controller has an integral track and hold amplifier with indefinite hold time capability, to enable immediate LED on cycles after extended off times. During extended off times, the external LEDs cool down from their normal quiescent operating temperature and thereby experience a forward voltage change, typically an increase in the forward voltage. This change can be significant for applications with a large number of series LEDs in a string operating at high current. If the boost controller did not track this increased change, the potential on the LED drivers would saturate for a few cycles once the LED channels are reenabled.

Also the device has a precharge voltage that add 0.5 Volts to the Boost, cycle by cycle of the PWM. It helps the boost to respond faster every time the load turns back on again.

#### **CURRENT MIRROR**

The programmable current mirror matches the current in 10 LED strings to within 2%. The maximum current is set using a resistor to GND from the ISET pin. This can be scaled down using the  $I^2C$  interface to 255 levels.

Zero current is achieved by turning off the LED Driver by  $I^2C$  (registers CHENx = 0 h) for a duty cycle from 0% to 99% or by pulling PWM pin low regardless of the duty cycle.

I<sup>2</sup>C capability allows the channels to be controlled individually or in parallel.

<span id="page-17-0"></span>**Current on LED Channel (PIN and NIN mode disabled) Eqn. 1**

Current[A] =  $\frac{|CH[RegisterValue]}{RSET[ohms]}$ 

In the off state, the LEDs current is set to 0 and the boost converter stops switching.

This feature allows to drive more than 50 mA of current by connecting the LED string to 2 or more LED channels in parallel. For example; if the application requires to drive 5 channels at 100 mA, then the bottom of each LED string should be connected to two channels in order to duplicate the current capability (Example: CH0+CH1 = 100 mA).

### **PWM GENERATOR**

The PWM generator can operate in either master or slave modes, as set by the M/~S pin.

In master mode, the internal PWM generator frequency is programmed through the  $I^2C$  interface (registers FPWM). The default programmed value set the number of 25 kHz clocks (40 μs) in one PWM cycle. The 18-bit resolution allows minimum PWM frequencies of 100 Hz to be programmed. The resulting frequency is output on the CK pin.

#### **PWM Frequency Eqn. 2**

 $\mathsf{PWMFrequency}[\mathsf{Hz}] = \frac{19.2\mathsf{Mhz}}{\mathsf{FPWM}[\mathsf{RegisterValue}]}$ 

In slave mode, the CK pin acts as an input. The internal digital PLL uses this frequency as the PWM frequency. By setting one device as master, and connecting the CK output to the input on a number of slave configured devices, all PWM frequencies are synchronized together.

The duty cycle of the PWM waveform in both master and slave modes is set using a second register on the  $I^2C$ interface (register DPWM), and can be controlled from 100% duty cycle to  $1/256$  T<sub>PWM</sub> = 0.39%. Zero percent of duty cycle is achieved by turning LED drivers off (register CHENx = 0h) or pulling PWM pin low.

An external PWM can also be used. The PWM input is 'AND'ed with the internal signal. By setting the serial interface to 100% duty cycle (default), the external pin has full control of the PWM duty cycle. This pin can also be used to modulate the LED at a lower frequency than the PWM dimming frequency (Minimum pulse width = 150 ns).

A pulsed mode can also be programmed using the  $I^2C$ interface (STROBE bit = 1). In this mode, each rising edge of the PWM signal turns on the next channel, while turning off all other channels. The duration that the channel is illuminated is set by the duty cycle of the PWM input pin. This can be used to scan the output channels.

#### **DISABLING LED CHANNELS**

The 34844 allows the user to enable and disable each of the 10 channels separately by writing the corresponding CHENx bit on Registers 08 and 09 thru  ${}^{12}$ C.

When a channel is disabled thru the  $I^2C$  prior the device starts to operate, the corresponding LED driver is disabled but the feedback circuit is still connected. This may interfere with the operation of the dynamic headroom control (DHC) which can lead to erratic output voltage regulation. For this condition, the output voltage may ramp up to the OVP level if the voltage on the LED driver is not substantially above the DHC regulation voltage (0.75 V typ). Because of this operation under I<sup>2</sup>C/SMBUS Mode, we recommend to connect the unused channels to VDC2 thru a100 kohm resistor and also follow the below powering up sequence:

- 1. PWM pin = Low.
- 2. Power up the part.
- 3. Program the  $I^2C$  commands and disable the unused channels.
- 4. Enable the Boost and current drivers by taking PWM pin to HIGH.

This previous device's operation does not happen when all channels are being used because the voltage across the LED drivers is always equal or higher than the DHC regulation voltage (0.75 V typ). For this condition, the user can disable/ enable any of the channels thru  $I^2C$  without causing any erratic behavior but the FAIL pin cannot be cleared. If FAIL pin is to be cleared thru  $I^2C$ , it will be necessary to use the suggested configuration shown at the FAIL PIN session.

### **FAIL PIN**

If a LED fails open in any of the LED strings, the voltage in that particular LED channel will be close to ground and the LED open failure is detected. When this happens, a failure is registered, the FAIL pin is set to its high-impedance stage, and the channel is turned off.

The FAIL pin cannot be cleared for manual mode unless a complete power on reset is applied. However for I<sup>2</sup>C/SMBUS mode, the FAIL pin is cleared by disabling the malfunction channels (CHENx = 0) and clearing the failure bit (CLRFAIL  $bit = 1$ ).

If the application only requires clearing the failure for the floating or unused channels, then the unused channels must be connected to VDC2 thru a 100 kohm resistor to avoid reach instability problems. This will allow detecting another failure from the connected channels. (See [Figure 6](#page-18-0))



#### **Figure 6. Single Channel Disconnect Circuit.**

<span id="page-18-0"></span>For applications where multiple failure detection is required, then one 100 kohm resistor must be placed from each channel to a diode (D2) connected to VDC2. The resistor will provide a pull up voltage to the disconnected channels so that they do not interfere with the DHC circuit. The diode (D2) ensures that when the connected channels are in PWM off state the LED strings do no conduct current to VDC2. (See [Figure 7\)](#page-18-1)



#### <span id="page-18-1"></span> **Figure 7. Resistor/Diode placement for multiple open circuit detection**

If the fail pin cannot be cleared by software then it indicates that the failure is because of t an over-current in the Boost.

Since this is a critical failure the only way to clear it is by releasing the part from the over-current condition and then shutdown the part (Refer to [Table 5\)](#page-16-0)

If I<sup>2</sup>C communication is not present, FAIL condition should be reset by removing the failure and re-enabling the device thru the EN pin.

#### **OPTICAL AND TEMPERATURE CONTROL LOOP**

The 34844 supports both optical and temperature loop control.

For temperature loop control, the LED brightness can be adjusted depending on the temperature of the LEDs.

For optical loop control, the 34844 supports both optical closed loop backlight control, where the brightness of the backlight is maintained at a required level by adjusting the light output, until the desired level is achieved, or with ambient light control, where the backlight brightness increases as ambient light increases.

Both temperature and optical loops are supported through the PIN and NIN pins. Each pin supports a 0-2.048 V input range which affects the current through the LEDs. The PIN pin increases current as the voltage rises from 0-2.048 V. The NIN pin reduces current as the voltage rises from 0- 2.048 V.

A 10.2 k resistor or higher value must be used at the ISET pin if the part is configured to use PIN+NIN control loop functionality, the 50 mA maximum current is achieved at the higher allowed level of PIN/NIN pins, ensuring the maximum current of the LED Drivers are not exceeded.

The optical and temperature control loop can be disabled by I<sup>2</sup>C setting bits (PINEN & NINEN), or by tying PIN and NIN pins high (>2.2 V) it is called  $V_{\text{SFT}}$  mode, and the LED Driver maximum current is set to 50 mA by using a 5.1 k resistor at the ISET pin.



 $Current[A] = \frac{(2.048 - VNIN) \times ICH[RegisterValue]}{I}$  $RSET[ohms] \times 2$ 

**Current on LED Channel (PIN+NIN mode) Eqn. 5**

 $Current[A] = \frac{(2.048 - VNIN + VPIN) \times ICH[RegisterValue]}{$  $RSET[ohms] \times 2$ 

## **LED FAILURE PROTECTION**

#### **Open LED Protection**

If LED fails open in any of the LED strings, the voltage in that channel will be pulled close to zero, which will cause the channel to be disabled. As a result, the boost output voltage will go to the OVP level and then come down to the regulation level to continue powering the rest of the LED strings.

#### **Short LED Protection**

If an LED shorted in any of the LED strings, the device will continue to operate without interruption. However, if the

shorted LED happens to be in the LED string with the highest forward voltage, the DHC circuit will automatically regulate the output voltage with respect to the new highest LED voltage. If more LEDs are shorted in the same LED string, it may cause excessive power dissipation in the channel which may cause the OTT circuit to trip which will completely shutdown the device.

## **OVER-TEMPERATURE PROTECTION**

The 34844 has an on-chip temperature sensor that measures die temperature. If the IC temperature exceeds the OTT threshold, the IC will turn off all power sources inside the IC (LED drivers, boost and internal regulators) until the

temperature falls below the falling OTT threshold. Once it comes back on, it will operate with the default configuration (refer to [Table 7](#page-22-0)).

### **SERIAL INTERFACE CONTROL**

The 34844 uses an  $I^2C$  interface capable of operating in standard (100 kHz) or fast (400 kHz) modes.

The A0/SEN pin can be used an address select pin to allow more than 2 devices in the system. The A0/SEN pin should be held low on all chips expect the one to be addressed, where it is taken HIGH.

## **FUNCTIONAL DEVICE OPERATION**

#### *OPERATIONAL MODES*

#### <span id="page-20-0"></span>**NORMAL MODE**

In normal operation the 34844 is programed via  $I^2C$  to drive up to 50 mA of current through each one of the LED channels. The 34844 can be configured in master or slave mode as set by the M/~S pin.

In **Master mode**, the internal PWM generator frequency is programmed through the I<sup>2</sup>C interface. The programmed value sets the number of 25 kHz clocks (40μs) in one PWM cycle. The 18-bit resolution allows minimum PWM frequencies of 100 Hz to be programmed. The resulting frequency is output on the CK pin.

In slave mode, the CK pin acts as an input. The internal digital PLL uses this frequency as the PWM frequency.

By setting one device as a master, and connecting the CK output to the input on a number of slave configured devices, all PWM frequencies are synchronized together. For this application A0/SEN pin indicates which device is enable for  $I^2$ C control.

In **Slave mode**, an internal phase lock loop will lock the internal PWM generator period to the period of the signal present at the CK pin. The PLL can lock to any frequency from 100 Hz to 25 KHz provided the jitter is below 1000 ppm. At frequencies above 1.0 KHz, the PLL will maintain lock regardless of the transient power conditions imposed by the user (i.e. going from 0% duty cycle to 100% at 20W LED display power). Below 1.0 kHz, thermal time constants on the die are such that the PLL may momentarily lose lock if the die temperature changes substantially during a large load power step. As explained below, this anomaly can be avoided by controlling the rate of change in PWM duty cycle.

To better understand this issue, consider that the on chip PLL uses a VCO that is subject to thermal drift on the order of 1000 ppm/C. Further consider that the thermal time constant of the chip is on the order of single digit milliseconds. Therefore, if a large power load step is imposed by the user (i.e. going from 0% duty cycle to 100% duty cycle with a load power of 20 W), the die will experience a large temperature wave gradient that will propagate across the chip surface and thereby affect the instantaneous frequency of the VCO. As long as such changes are within the bandwidth of the PLL, the PLL will be able to track and maintain lock. Exceeding this rate of change may cause the PLL to lose lock and the backlight will momentarily be blanked until lock is reacquired.

At 100 Hz lock, the PLL has a bandwidth of approximately 10 Hz. This means that temperature changes on the order of 100 ms are tolerable without losing lock. But full load power changes on the order of 10 ms (i.e. 100 Hz PWM) are not tracked out and the PLL can momentarily lose lock. If this happens, as stated above, the LED drivers are momentarily disabled until lock is reacquired. This will be manifested as a

perceivable short flash on the backlight immediately after the load change.

To avoid this problem, one can simply limit large instantaneous changes in die temperature by invoking only small power steps when raising or lowering the display power at low PWM frequencies. For example, to maintain lock while transitioning from 0% to 100% duty cycle at 20 W load power and a PWM frequency of 100 Hz would entail stepping the power at a rate not to exceed 1% per 10 ms. If a load of less than 20 W is used, then the rate of rise can be increased. As the locked PWM frequency increases (i.e. use 600 Hz instead of 100 Hz), the step rate can be further increased to approximately 4% per 2.0 ms. The exact step rate to avoid loss of PLL lock is a function of essentially three things: (a) the composite thermal resistance of the user's PCB assembly, (b) the load power, and (c) the PWM frequency. For all cases below 1.0 KHz, simply using a rate of 1% duty cycle change per PWM period will be adequate. If this is too slow, the value can be optimized experimentally once the hardware design is complete. At PWM rates above 1.0 KHz, it is not necessary to control the rate of change in PWM duty cycle.

It is important to point out that when operating in the master mode, one does not need to concern themselves with loss of lock since the reference clock and the VCO clock are collocated on the die, and therefore experience the same thermal shift. Hence in master mode, once lock is initially acquired, it is not lost and no blanking of the display occurs.

The duty cycle of the PWM in both master and slave mode is set using a second register on the  $I<sup>2</sup>C$  interface.

An external PWM signal can also be applied in the PWM pin. This pin is AND'ed with the internal signal, giving the ability to control the duty cycle either via  $I^2C$  or externally by setting any of the 2 signals to 100% duty cycle.

#### **STROBE MODE**

A strobe mode can be programmed via  $I^2C$ .

In this mode, each rising edge of the PWM signal turns on the next channel, while turning off all other channels. The duration that the channel is illuminated is set by the duty cycle of the PWM input pin.

This mode can be also programmed by controlling the ON and OFF state of each LED channel via  $1^2C$ .

#### **MANUAL MODE**

The 34844 can also be used in Manual mode without using the  $I^2C$  interface. By setting the pin M/ $\sim$ S High, the LED dimming will be controlled by the external PWM signal. The over-voltage protection limit can be settled by a resistor divider on A0/SEN pin.

During manual mode, all internal Registers are in Default Configuration, refer [Table 7,](#page-22-0) under this configuration the PIN and NIN pins are enabled to scale the current capability per string and may be disable by setting 2.2 V in the corresponding pin.

Also in this mode, the device can be enabled as follows:

+ EN pin + PWM signal (Two Signals): In this configuration, the PWM signal applied to PWM pin will be in

charge of controlling the LED dimming and a second signal will enable or disable the chip through the EN pin. [Figure](#page-30-0) 21

+ PWM Signal tied to SDA pin (Just ONE signal): In this configuration the PWM pin should be tied to SDA pin. The

PWM signal applied to PWM pin will be in charge of controlling LED dimming and enable the device every time the PWM is active. For this configuration EN pin should be LOW.

### **POWER DOWN MODE**

If the input voltage falls below the UVLO threshold, the device enters automatically into power down mode. When in power down, the supply current is reduced below 2.0 μA when there is no  $I^2C$  activity, and it rises up when  $I^2C$ interface is enabled.

## *I <sup>2</sup>C BUS SPECIFICATION*

The 34844 is a unidirectional device that can only be written by an external control unit. Since the device is a 7 bit address device (1110110), the control unit needs to follow a specific data transfer format which is shown in [Figure 8.](#page-21-0)



#### **Figure 8. A Complete Data Transfer**

<span id="page-21-0"></span>For a complete data transfer, please use this format in the following order:

- 1. START condition
- 2. The 34844 device address and Write instruction  $(R/W = 0)$
- 3. First data pack, it corresponds to the 34844 Register that needs to be written. (refer to [Table](#page-22-1))
- 4. Second data pack, it corresponds to the value that should be written to that register. (refer to **Table**)
- 5. STOP condition

<sup>2</sup>C variables description:

- START: this condition occurs when SDA changes from HIGH to LOW while SCK is HIGH.
- ACKNOWLEDGE: The acknowledge clock pulse is generated by the Master (Control Unit).
- The transmitter releases the SDA line (HIGH) during the acknowledge clock pulse.

The receiver (34844) must pull down the SDA line during this acknowledge pulse to indicate that the data was correctly written.

Bits in the first byte: The first seven bits of the first bite make up the slave address. The eighth bit is the LSB (least significant bit), which determines the direction of the message (Write = 0)

For the 34844 device, when an address is sent, each of the devices in a system compares the first seven bits after the START condition with its address. If they match, the device considers itself addressed by the control unit as a slave-receiver.

STOP: this condition occurs when SDA changes from LOW to HIGH while SCK is HIGH

For more information about "I<sup>2</sup>C BUS SPECIFICATION" please refer to the following link:

http://www.nxp.com/acrobat\_download/literature/ 9398/39340011.pdf

**34844**

## *LOGIC COMMANDS AND REGISTERS*

### **Table 6. Write Registers**



### <span id="page-22-1"></span><span id="page-22-0"></span>**Table 7. Register Description**





### **Table 7. Register Description**

**Table 8. Over-voltage Protection**





*TYPICAL PERFORMANCE CURVES (TA=25°C)*

 **Figure 9. Boost efficiency vs Input Voltage**



 **Figure 10. Line Regulation, V<sub>IN</sub> Changing** 







 **Figure 12. Bias Current vs Input Voltage (Operational Mode)**



 **Figure 13. Bias Current vs Input Voltage (Sleep Mode)**



 **Figure 14. Boost Soft Start**



 **Figure 15. Typical Operation Waveforms for FPWM=600 Hz, 40% Duty**



 **Figure 16. Typical Operation Waveforms for FPWM=600 Hz, 100% Duty**



 **Figure 17. Low Duty Dimming Operation Waveforms (FPWM=20 kHz, 2LSB)**



 **Figure 18. Low Duty Dimming Operation Waveforms (FPWM=20 kHz, 1LSB)**

# **TYPICAL APPLICATIONS**



### **Figure 19. Manual Mode (Single Wire Control)**



MANUAL MODE (Two Wire Control)

 **Figure 20. Manual Mode (Two Wire Control)**



 **Figure 21. SM Bus Mode**



<span id="page-30-0"></span>

 **Figure 22. Master - Slave Connection**

## <span id="page-31-0"></span>**MC34844A SPECIFICATIONS PAGES 32 TO 54**



# **INTERNAL BLOCK DIAGRAM**

 **Figure 23. 34844A Simplified Internal Block Diagram**

## **PIN CONNECTIONS**



#### **Figure 24. 34844A Pin Connections**

# **Table 9. 34844A Pin Definitions**

A functional description of each pin can be found in the Functional Pin Description section beginning on [page](#page-41-0) 42.



#### **34844A**

### **Table 9. 34844A Pin Definitions (continued)**

A functional description of each pin can be found in the Functional Pin Description section beginning on page 42.



# **ELECTRICAL CHARACTERISTICS**

### *MAXIMUM RATINGS*

#### **Table 10. Maximum Ratings**

All voltages are with respect to ground unless otherwise noted. Exceeding these ratings may cause a malfunction or permanent damage to the device.



Notes

<span id="page-35-1"></span>14. ESD testing is performed in accordance with the Human Body Model (HBM) (AEC-Q100-2), and the Machine Model (MM) (AEC-Q100- 003),  $R_{ZAP} = 0 Ω$ 

<span id="page-35-2"></span>15. Per JEDEC51 Standard for Multilayer PCB

<span id="page-35-3"></span>16. Pin soldering temperature limit is for 10 seconds maximum duration. Not designed for immersion soldering. Exceeding these limits may cause malfunction or permanent damage to the device.

<span id="page-35-0"></span>17. 45 V is the Maximum allowable voltage on all LED channels in off-state.

## *STATIC AND DYNAMIC ELECTRICAL CHARACTERISTICS*

### **Table 11. Static and Dynamic Electrical Characteristics**

Characteristics noted under conditions  $V_{IN}$  = 12 V,  $V_{OUT}$  = 42 V, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1,  $-40^{\circ}$ C  $\leq$  T<sub>A</sub> $\leq$  105°C, PGND = 0 V, unless otherwise noted.



Notes

<span id="page-36-1"></span>18. This output is for internal use only and not to be used for other purposes. A 1.0 kΩ resistor between the VDC3 and VDC1 pin is recommended for <-20 °C operation.

Peak Boost Efficiency<sup>[\(20\)](#page-36-0)</sup> and the set of the set of the Second EFF<sub>BOOST</sub>  $\vert$  -  $\vert$  90  $\vert$  -  $\vert$  %

<span id="page-36-2"></span><span id="page-36-0"></span>19. Minimum and Maximum output voltages are dependent on Min/Max duty cycle and current limit condition.

#### ELECTRICAL CHARACTERISTICS *STATIC AND DYNAMIC ELECTRICAL CHARACTERISTICS*

### **Table 11. Static and Dynamic Electrical Characteristics (continued)**

Characteristics noted under conditions  $V_{IN}$  = 12 V,  $V_{OUT}$  = 42 V, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1,  $-40^{\circ}C \leq T_A \leq 105^{\circ}C$ , PGND = 0 V, unless otherwise noted.



<span id="page-37-0"></span>Notes

### **Table 11. Static and Dynamic Electrical Characteristics (continued)**

Characteristics noted under conditions  $V_{IN}$  = 12 V,  $V_{OUT}$  = 42 V, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1,  $-40^{\circ}C \leq T_A \leq 105^{\circ}C$ , PGND = 0 V, unless otherwise noted.



<span id="page-38-0"></span>Notes

#### MC34844A

#### ELECTRICAL CHARACTERISTICS *STATIC AND DYNAMIC ELECTRICAL CHARACTERISTICS*

### **Table 11. Static and Dynamic Electrical Characteristics (continued)**

Characteristics noted under conditions  $V_{IN}$  = 12 V,  $V_{OUT}$  = 42 V, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1, -40°C  $\leq$  T<sub>A</sub> $\leq$  105°C, PGND = 0 V, unless otherwise noted.



Minimum Duty Cycle **Development Contract C** Maximum Duty Cycle **DESA CONSERVERSE ASSESSED ASSES** Soft Start Period  $t_{SS}$  -  $\vert$  -  $\vert$  6.5 -  $\vert$  ms

Boost Switch Rise Time<sup>[\(23\)](#page-39-0)</sup> t<sub>TR</sub>  $t_{TR}$  15 - ns Boost Switch Fall Time<sup>[\(23\)](#page-39-0)</sup> t<sub>F</sub>

Notes

<span id="page-39-0"></span>23. Guaranteed by design

- | 25 | - | ns

### **Table 11. Static and Dynamic Electrical Characteristics (continued)**

Characteristics noted under conditions  $V_{IN}$  = 12 V,  $V_{OUT}$  = 42 V, PWM = VDC1, M/~S = VDC1, PIN & NIN = VDC1, -40°C  $\leq$  T<sub>A</sub> $\leq$  105°C, PGND = 0 V, unless otherwise noted.



Notes

<span id="page-40-1"></span>24. Special considerations should be made for frequencies between 110 Hz to 1.0 KHz. Please refer to [Functional Device Operation](#page-47-0) for further details.

<span id="page-40-0"></span>25. Guaranteed by design

**34844A**

# **FUNCTIONAL DESCRIPTION**

#### *INTRODUCTION*

LED backlighting has become very popular for small and medium LCDs, due to some advantages over other backlighting schemes, such as the widely used cold cathode fluorescent lamp (CCFL). The advantages of LED backlighting are low cost, long life, immunity to vibration, low operational voltage, and precise control over its intensity.

However, there is an important drawback of this method. It requires more power than most of the other methods, and this is a major problem if the LCD size is large enough.

To address the power consumption problem, solid state optoelectronics technologies are evolving to create brighter LEDs with lower power consumption. These new technologies together with highly efficient power management LED drivers are turning LEDs, a more suitable solution for backlighting almost any size of LCD panel, with really conservative power consumption.

One of the most common schemes for backlighting with LED is the one known as "Array backlighting". This creates a matrix of LEDs all over the LCD surface, using defraction and diffused layers to produce an homogenous and even light at the LCD surface. Each row or column is formed by a number of LEDs in series, forcing a single current to flow through all LEDs in each string.

Using a current control driver, per row or column, helps the system to maintain a constant current flowing through each line, keeping a steady amount of light even with the presence of line or load variations. They can also be use as a light intensity control by increasing or decreasing the amount of current flowing through each LED string.

To achieve enough voltage to drive a number of LEDs in series, a boost converter is implemented, to produce a higher voltage from a smaller one, which is typically used by the logical blocks to do their function.

The 34844A implements a single channel boost converter together with 10 input channels, for driving up to 16 LEDs per string to create a matrix of more than 160 LEDs. Together with its 90% efficiency and  $1<sup>2</sup>C$  programmable or external current control, among other features, makes the 34844A a perfect solution for backlighting small and medium size LCD panels, on low power portable and high definition devices.

### *FUNCTIONAL PIN DESCRIPTION*

### <span id="page-41-0"></span>**INPUT VOLTAGE SUPPLY (VIN)**

IC Power input supply voltage, is used internally to produce internal voltage regulation (VDC1, VDC3) for logic functioning, and also as an input voltage for the boost regulator.

### **INTERNAL VOLTAGE REGULATOR 1 (VDC1)**

This pin is for internal use only, and not to be used for other purposes. A capacitor of 2.2 μF should be connected between this pin and ground for decoupling purposes.

### **INTERNAL VOLTAGE REGULATOR 2 (VDC2)**

This pin is for internal use only, and not to be used for other purposes. A capacitor of 2.2 μF should be connected between this pin and ground for decoupling purposes.

#### **INTERNAL VOLTAGE REGULATOR 3 (VDC3)**

This pin is for internal use only, and not to be used for other purposes. A capacitor of 2.2 μF should be connected between this pin and ground for decoupling purposes. A 1.0 kΩ resistor between the VDC3 and VDC1 pin is recommended for <-20 °C operation.

#### **BOOST COMPENSATION PIN (COMP)**

Passive terminal used to compensate the boost converter. Add a capacitor and a resistor in series to GND to stabilize the system.

#### **IC ENABLE (EN)**

The active high enable terminal is internally pulled high through pull-up resistors. Applying 0V to this terminal would stop the IC from working.

#### **INPUT/OUTPUT CLOCK SIGNAL (CK)**

This terminal can be used as an output clock signal (master mode), or input clock signal (slave mode), to synchronize more than one device.

#### **MASTER/SLAVE MODE SELECTION (M/~S)**

Setting this pin High puts the device into Master mode, producing an output synchronization clock at the CK terminal. Setting this pin low, puts the device in Slave mode, using the CK pin as an input clock.

#### **EXTERNAL PWM INPUT (PWM)**

This terminal is internally pulled down. An external PWM signal can be applied to modulate the LED channel directly in absence of an  $I^2C$  interface.

## **CLOCK I2C SIGNAL (SCK)**

Clock line for I2C communication.

## **ADDRESS I2C SIGNAL (SDA)**

Address line for I<sup>2</sup>C communication.

**34844A**

### **A0/SEN**

Address select, device select pin, or Hardware Overvoltage Protection (OVP) Control.

#### **CURRENT SET (ISET)**

Each LED string can drive up to 50 mA. The maximum current can be set by using a resistor from this pin to GND.

#### **POSITIVE CURRENT SCALING (PIN)**

Positive current scaling factor for the external analog current control. Applying 0 V to this pin, scales the current to near 0%, and in the same way, applying  $V_{\text{SFT}}$  (2.048 V Typ.), the scale factor is 100%. By applying a voltage higher than 2.2 V, the scaling factor is disabled, and the internal pull-ups are activated.

If PIN pin and NIN pin are used at the same time then by applying 0 V to the PIN pin and  $V_{\text{SET}}$  to NIN pin, scales the current to near 0%, and in the same way, applying  $V_{\text{SFT}}$  to the PIN pin and 0 V to NIN pin, scales the current to 100%. By applying a voltage higher than 2.2 V, the scaling factor is disabled and the internal pull-ups are activated in both pins.

#### **NEGATIVE CURRENT SCALING (NIN)**

Negative current scaling factor for the external analog current control. Setting 0 V to this pin scales the current to 100%, in the same way, setting  $V_{\text{SET}}$  (2.048 V Typ.) the scale factor is near 0%. By applying a voltage higher than 2.2 V, the scaling factor is disabled and the internal pull-ups are activated.

If PIN pin and NIN pin are used at the same time then by applying 0 V to the PIN pin and  $V_{\text{SFT}}$  to NIN pin, scales the current to near 0%, and in the same way, applying  $V_{\text{SFT}}$  to the PIN pin and 0 V to NIN pin, scales the current to 100%. By

applying a voltage higher than 2.2 V, the scaling factor is disabled and the internal pull-ups are activated in both pins.

#### **GROUND (GND)**

Ground Reference for all internal circuits other than the Boost FET.

The Exposed Pad (EP) should be used for thermal heat dissipation.

#### **I0-I9**

Current LED driver, each line has the capability of driving up to 50 mA.

#### **FAULT DETECTION PIN (FAIL)**

When a fault situation is detected, this pin goes into high impedance.

#### **BOOST SLOPE COMPENSATION SETTING RESISTOR (SLOPE)**

The resistor to be used for the SLOPE depends on the Input and Output voltage difference as well as the inductor value. Please use the formula shown in the [Components](#page-54-0)  [Calculation](#page-54-0) section to calculate the value accordingly.

#### **POWER GROUND TERMINALS (PGNDA, PGNDB)**

Ground terminal for the internal Boost FET.

#### **OUTPUT VOLTAGE SENSE TERMINAL (VOUT)**

Input terminal to monitor the output voltage. It also supplies the input voltage for the internal regulator 2 (VDC2).

#### **SWITCHING NODE TERMINALS (SWA, SWB)**

Switching node of boost converter.



### *FUNCTIONAL INTERNAL BLOCK DESCRIPTION*



### **REGULATORS**

The 34844A is designed to operate from input voltages in the 7.0 to 28 V range. This is stepped down internally by LDOs to 2.5 V (VDC1 and VDC3) and 6 V (VDC3) for powering internal circuitry. If the input voltage falls below the UVLO threshold, the device automatically enters in shut down mode.

#### **Power UP Sequence:**

The power up sequence for applying  $V_{IN}$ , with respect to the ENABLE and PWM signals, is very important to assure a good performance of the part.

- It is recommended to follow this sequence:
- 1. Apply  $V_{IN}$  first
- 2. Wait for a couple of milliseconds (~2.0 ms) to let the logic and internal regulators get settled
- 3. Take the EN pin high, or keep it low depending on the operating mode
- 4. Apply the PWM signal

#### **Operating Modes:**

The device can be operated by the EN pin and/or SDA/ SCK bus lines, resulting in three distinct operation modes:

- Manual mode, there is no  $1^2C$  capability, the bus line pins must be tied low, and the EN pin controls the ON/OFF operation. To shutdown the part in Manual mode, first the PWM pin should be taken low followed by the EN pin. The part will not shut down unless  $V_{OUT}$  collapses to a voltage below 30 V.
- SM Bus mode, EN pin must be tied low and the device is turned ON by any activity on the bus lines. The part shuts down if the bus lines are held low for more than 30 ms, the 30 ms watchdog timer can be disabled by  $I^2C$  (setting SETI2C bit high) or tying the EN pin high. In Sleep mode (EN bit=0) the device reduces the power consumption by leaving "alive" only the blocks required for  $I<sup>2</sup>C$ communication.To shutdown the part in SM Bus mode, the EN bit should first be a '0', then the SCK and SDA should be taken low.
- $\cdot$  I<sup>2</sup>C mode, has to be configured by I<sup>2</sup>C communication (SETI2C bit = 1) right after the IC is turned ON, it prevents the part from being turned ON/OFF by the bus. Sleep mode is also present and it is intended to save power, but still keep the IC prepared to communicate by  $I^2C$ . By taking the EN bit low and then the EN pin low, the part enters into a shutdown mode.

<b>MODE</b>	<b>EN Pin</b>	<b>SCK/SDA Pins</b>	<sup>2</sup> C Bit Command	<b>Current Consumption</b> Mode	<b>Comments</b>
Manual	Low	Low	N/A	Shutdown	PWM pin = Low
	High	Low	N/A	Operational	
SM Bus	Low	Low $(> 27$ ms)	$EN bit = 0$	Shutdown	
	Low	Active	$EN bit = 0$	Sleep	
	Low	Active	$EN bit = 1$	Operational	
$I^2C$	Low	X	SETI2C bit = $1$	<sup>2</sup> C Low Power (Shutdown)	Part Doesn't Wake-up
			CLRI2C bit = $0$		
			$EN bit = 0$		
	High	X	SETI2C bit = $1$		
			CLRI2C bit = $0$	Sleep	
			$EN bit = 0$		
	High	X	SETI2C bit = $1$	Operational	
			CLRI2C bit = $0$		
			$EN bit = 1$		

<span id="page-44-0"></span>**Table 12. Operation Current Consumption Modes**

#### **BOOST**

The integrated boost converter operates in nonsynchronous mode and integrates a 2.5 A FET. An integrated sense circuit is used to sense the voltage at the LED current mirror inputs and automatically sets the boost output voltage (DHC) to the minimum voltage needed to keep all LEDs biased with the required current. The DHC is designed to operate for pulse widths > 400 ns in the LED drivers.

If the pulse widths are shorter than specified, the DHC circuit will not operate and the voltage across the LED drivers will increase to a value given by the OVP minus the total LED voltage in the LED string. Therefore it is imperative to select the proper OVP level to minimize power dissipation.

The user can program the boost frequency by  $I^2C$ (BST[1:0]) only after the IC is powered up and before the boost circuit is turned ON for the first time (PWM pin low to high). This sequence avoids boost frequency to be changed inadvertently during operation. The first  $I^2C$  command has to wait for 5.0 ms after the part is turned ON, in order to allow sufficient time for the device power up sequence to be completed.

Please follow this sequence in order to change the Boost frequency thru I2C:

- 1. Take PWM pin low
- 2. Disable the part by software (EN bit = low)
- 3. Write the new Boost frequency data (BST[1:0])
- 4. Enable the part by software (EN bit = high)
- 5. Reconfigure all registers
- 6. Take PWM pin High

The boost controller has an integral track and hold amplifier with indefinite hold time capability, to enable immediate LED on cycles after extended off times. During extended off times, the external LEDs cool down from their normal quiescent operating temperature and thereby experience a forward voltage change, typically an increase in the forward voltage. This change can be significant for applications with a large number of series LEDs in a string operating at high current. If the boost controller did not track this increased change, the potential on the LED drivers would saturate for a few cycles once the LED channels are reenabled.

#### **HARDWARE AND SOFTWARE OVP**:

The OVP value should be set to a higher value than the maximum LED voltage over the whole temperature range. A good practice is to set it 5.0 V or so above the max LED voltage.

The OVP can be set from 11 to 62 V, ~4.0 V spaced, using the  $I^2C$  interface (OVP Register). If the  $I^2C$  capability is not present, the OVP can be controlled either by a resistor divider connected from VOUT to GND, with its mid point tied to the A0/SEN pin, or by a zener diode from VOUT to the A0/SEN pin (threshold =  $6.5$  V). During an OVP condition, the output voltage will go to the OVP level, which is programmed via the <sup>2</sup>C interface or settled by a resistor divider on A0/SEN pin, or by a zener diode. The formulas to calculate the hardware OVP using any of the two methods are as follows:



 $OVP = 6.5 V [(R_{UPPER} / R_{LOWER}) + 1] + (100E-6 K R_{UPPER})$ 

### **OVER-CURRENT PROTECTION (OCP)**

The boost converter also features internal Over-current Protection (OCP) and has a user programmable Overvoltage Protection (OVP).

The OCP operates on a cycle by cycle basis. However, if the OCP condition remains for more than 10ms then the device turns off the LED Drivers, the Boost goes to Sleep mode and the output FAULT pin goes into high-impedance. The device can only be restarted by recycling the enable or creating a Power On Reset (POR).

#### **CURRENT MIRROR**

The programmable current mirror matches the current in 10 LED strings to within 2%. The maximum current is set using a resistor to GND from the ISET pin. This can be scaled down using the  $I^2C$  interface to 255 levels.

Zero current is achieved by turning off the LED Driver by  $1^2C$  (registers CHENx = 0h) for a duty cycle from 0% to 99%, or by pulling PWM pin low regardless of the duty cycle.

 $I<sup>2</sup>C$  capability allows the channels to be controlled individually or in parallel.

**Current on LED Channel (PIN and NIN mode disabled) Eqn. 6**

$$
ISINK[A] = \frac{VSET[V] \times 136}{RISET[\Omega]} \times \frac{ICH[RegisterValue]}{255}
$$

Default ICH[RegisterValue]=255

In the off state, the LEDs current is set to 0 and the boost converter stops switching.

This feature allows to drive more than 80 mA of current by connecting the LED string to 2 or more LED channels in parallel. For example; if the application requires to drive a channels at 160 mA, then the bottom of each LED string should be connected to two channels in order to duplicate the current capability (Example: CH0+CH1 = 160 mA).

### **PWM GENERATOR**

The PWM generator can operate in either master or slave modes, as set by the M/~S pin.

In master mode, the internal PWM generator frequency is programmed through the  $I^2C$  interface (registers FPWM). The default programmed value set the number of 27 kHz clocks (40 μs) in one PWM cycle. The 18-bit resolution allows minimum PWM frequencies of 110 Hz to be programmed. The resulting frequency is output on the CK pin.

**Eqn. 7** 

$$
FPWM[Hz] = \frac{20.736Mhz}{FPWM[RegisterValue]}
$$

In slave mode, the CK pin acts as an input. The internal digital PLL uses this frequency as the PWM frequency. By setting one device as master, and connecting the CK output to the input on a number of slave configured devices, all PWM frequencies are synchronized together.

The duty cycle of the PWM waveform in both master and slave modes is set using a second register on the  $I^2C$ interface (register DPWM), and can be controlled from 100% duty cycle to 1/256 Tpwm = 0.39%. Zero percent of duty cycle is achieved by turning LED drivers off (register CHENx = 0h) or pulling PWM pin low.

An external PWM can also be used. The PWM input is 'AND'ed with the internal signal. By setting the serial interface to 100% duty cycle (default), the external pin has full control of the PWM duty cycle. This pin can also be used to modulate the LED at a lower frequency than the PWM dimming frequency (DHC Minimum pulse width = 400 ns).

#### <span id="page-45-0"></span>**POWER OFF AND POWER ON LED CHANNELS**

The 34844A allows the user to Power OFF and Power ON any channel independently thru I2C/SM-BUS mode.

The POWER ON function reconnects the LED driver and the feedback circuit to the channel to allow functionality to that channel again.

On an opposite way when the channel is POWER OFF, the LED driver and feedback circuit are disconnected to the channels.

This function is very useful for applications where one or more channel has to be shutdown to avoid the output voltages goes to OVP during the start up of the part.

The sequence to make these functions work is the following:

- To POWER ON LED channels:
- 1. Take PWM pin low
- 2. Set POWER ON bit high (MSB of Register 09)
- 3. Set high all Channels that should be power on by writing "1" on CHENx bits (Registers 08 & 09)
- 4. Clear POWER ON bit
- 5. Take PWM pin high

To POWER OFF LED channels:

- 1. Take PWM pin low
- 2. Set POWER OFF bit high (MSB of Register 08)
- 3. Clear all Channels that should be power off by writing "0" on CHENx bits (Registers 08 & 09)
- 4. Clear POWER OFF bit
- 5. Take PWM pin high

POWER ON bit and POWER OFF bit shouldn't be set at the same time in order to avoid damage to the part.

POWER ON/OFF channels should be reconfigured every time the part gets recovered from a POR or shutdown condition. This also apply if the part is reenabled by software.

If the part is reenabled by software, it is recommended to take PWM pin low, reenable the part and then follow the corresponding sequence shown above.

### **DISABLING LED CHANNELS**

The 34844A allows the user to enable and disable each of the 10 channels separately by writing the corresponding CHENx bit on Registers 08 and 09 thru I2C.

Since the enable and disable functions reconnects the feedback circuit of the LED drivers, this shouldn't be used on any channel that shuts down either because an open LED channel condition or because is was previously POWER OFF. This could cause instability issues since the voltage on this open LED driver is not substantially above the DHC regulation voltage (0.75 V typ) and may interfere with the operation of the dynamic headroom control (DHC) which can lead to erratic output voltage regulation

#### **FAIL PIN**

If a LED fails open in any of the LED strings, the voltage in that particular LED channel will be close to ground and the LED open failure is detected. When this happens, a failure is registered, the FAIL pin is set to its high-impedance stage, and the channel is shut down.

The FAIL pin cannot be cleared for manual mode unless a complete power on reset is applied.

However for I<sup>2</sup>C/SMBUS mode, the FAIL pin can be cleared by cycling the clear fail bit (CLRFAIL bit  $= 0 - 1 - 0$ ). This allows the user to waive any known failure and set the device for being able to detect any other failure during operation.

If the fail pin cannot be cleared by software then it indicates that the failure is because of an over-current in the Boost. Since this is a critical failure the only way to clear it is by releasing the part from the over-current condition and then shutdown the part (Refer to **Table 12)** 

If I<sup>2</sup>C communication is not present, FAIL condition should be reset by removing the failure and re-enabling the device thru the EN pin.

#### **OPTICAL AND TEMPERATURE CONTROL LOOP**

The 34844A supports both optical and temperature loop control.

For temperature loop control, the LED brightness can be adjusted depending on the temperature of the LEDs.

For optical loop control, the 34844A supports both optical closed loop backlight control, where the brightness of the backlight is maintained at a required level by adjusting the light output, until the desired level is achieved, or with ambient light control, where the backlight brightness increases as ambient light increases.

Both temperature and optical loops are supported through the PIN and NIN pins. Each pin supports a 0 V to  $V_{\text{SFT}}$ (2.048 V typ.) input range which affects the current through the LEDs. The PIN pin increases current as the voltage rises from 0 to  $V_{\text{SET}}$ . The NIN pin reduces current as the voltage rises from  $0 - V_{\text{SFT}}$ .

A 6.98 kohm resistor or higher value must be used at the ISET pin if the part is configured to use PIN+NIN control loop

functionality, the 80 mA maximum current is achieved at the higher allowed level of PIN/NIN pins, ensuring the maximum current of the LED Drivers are not exceeded.

The optical and temperature control loop can be disabled by I<sup>2</sup>C setting bits (PINEN & NINEN), or by tying PIN and NIN pins high (>2.2 V). The LED Driver maximum current is set to 80 mA by using a 3.48 kohm resistor at the ISET pin.

Current on LED Channel (PIN mode) Eqn. 8  
\n
$$
IDIM[A] = ISINK[A] \times \frac{VPIN[V]}{2}
$$
\n  
\nCurrent on LED Channel (NIN mode) Eqn. 9

$$
IDIM[A] = ISINK[A] \times \frac{(VSET - VNIN)[V]}{2}
$$

**Current on LED Channel (PIN+NIN mode) Eqn. 10**  $IDIM[A] = ISINK[A] \times \frac{(VSET+VPIN-VNIN)[V]}{2}$ 

VPIN and VNIN is the voltage applied on PIN and NIN pins correspondingly.

For ISINK formula please refer to **Equation 1.** 

### **LED FAILURE PROTECTION**

#### **Open LED Protection**

If LED fails open in any of the LED strings, the voltage in that channel will be pulled close to zero, which will cause the channel to be disabled. As a result, the boost output voltage will go to the OVP level and then come down to the regulation level to continue powering the rest of the LED strings.

#### **Short LED Protection**

If an LED shorted in any of the LED strings, the device will continue to operate without interruption. However, if the shorted LED happens to be in the LED string with the highest forward voltage, the DHC circuit will automatically regulate the output voltage with respect to the new highest LED voltage. If more LEDs are shorted in the same LED string, it may cause excessive power dissipation in the channel which may cause the OTT circuit to trip which will completely shutdown the device.

#### **OVER-TEMPERATURE PROTECTION**

The 34844A has an on-chip temperature sensor that measures die temperature. If the IC temperature exceeds the OTT threshold, the IC will turn off all power sources inside the IC (LED drivers, boost and internal regulators) until the temperature falls below the falling OTT threshold. Once it comes back on, it will operate with the default configuration (refer to [Table](#page-49-0) 14).

#### **SERIAL INTERFACE CONTROL**

The 34844A uses an  $I^2C$  interface capable of operating in standard (100 kHz) or fast (400 kHz) modes.

The A0/SEN pin can be used an address select pin to allow more than 2 devices in the system. The A0/SEN pin should be held low on all chips expect the one to be addressed, where it is taken HIGH.

## **FUNCTIONAL DEVICE OPERATION**

### *OPERATIONAL MODES*

#### <span id="page-47-0"></span>**NORMAL MODE**

In normal operation the 34844A is programed via  $I^2C$  to drive up to 50 mA of current through each one of the LED channels. The 34844A can be configured in master or slave mode as set by the M/~S pin.

In **Master mode**, the internal PWM generator frequency is programmed through the  $I^2C$  interface. The programmed value sets the number of 27 kHz clocks  $(37<sub>µ</sub>s)$  in one PWM cycle. The 18-bit resolution allows minimum PWM frequencies of 110 Hz to be programmed. The resulting frequency is output on the CK pin.

In slave mode, the CK pin acts as an input. The internal digital PLL uses this frequency as the PWM frequency.

By setting one device as a master, and connecting the CK output to the input on a number of slave configured devices, all PWM frequencies are synchronized together. For this application A0/SEN pin indicates which device is enable for  $I^2C$  control.

In **Slave mode**, an internal phase lock loop will lock the internal PWM generator period to the period of the signal present at the CK pin. The PLL can lock to any frequency from 110 Hz to 27 KHz provided the jitter is below 1000 ppm. At frequencies above 1.0 KHz, the PLL will maintain lock regardless of the transient power conditions imposed by the user (i.e. going from 0% duty cycle to 100% at 20W LED display power). Below 1.0 kHz, thermal time constants on the die are such that the PLL may momentarily lose lock if the die temperature changes substantially during a large load power step. As explained below, this anomaly can be avoided by controlling the rate of change in PWM duty cycle.

To better understand this issue, consider that the on chip PLL uses a VCO that is subject to thermal drift on the order of 1000 ppm/C. Further consider that the thermal time constant of the chip is on the order of single digit milliseconds. Therefore, if a large power load step is imposed by the user (i.e. going from 0% duty cycle to 100% duty cycle with a load power of 20 W), the die will experience a large temperature wave gradient that will propagate across the chip surface and thereby affect the instantaneous frequency of the VCO. As long as such changes are within the bandwidth of the PLL, the PLL will be able to track and maintain lock. Exceeding this rate of change may cause the PLL to lose lock and the backlight will momentarily be blanked until lock is reacquired.

At 110 Hz lock, the PLL has a bandwidth of approximately 10 Hz. This means that temperature changes on the order of 100 ms are tolerable without losing lock. But full load power changes on the order of 10 ms (i.e. 110 Hz PWM) are not tracked out and the PLL can momentarily lose lock. If this happens, as stated above, the LED drivers are momentarily disabled until lock is reacquired. This will be manifested as a perceivable short flash on the backlight immediately after the load change.

To avoid this problem, one can simply limit large instantaneous changes in die temperature by invoking only small power steps when raising or lowering the display power at low PWM frequencies. For example, to maintain lock while transitioning from 0% to 100% duty cycle at 20 W load power and a PWM frequency of 110 Hz would entail stepping the power at a rate not to exceed 1% per 10 ms. If a load of less than 20 W is used, then the rate of rise can be increased. As the locked PWM frequency increases (i.e. use 600 Hz instead of 110 Hz), the step rate can be further increased to approximately 4% per 2.0 ms. The exact step rate to avoid loss of PLL lock is a function of essentially three things: (a) the composite thermal resistance of the user's PCB assembly, (b) the load power, and (c) the PWM frequency. For all cases below 1.0 KHz, simply using a rate of 1% duty cycle change per PWM period will be adequate. If this is too slow, the value can be optimized experimentally once the hardware design is complete. At PWM rates above 1.0 KHz, it is not necessary to control the rate of change in PWM duty cycle.

It is important to point out that when operating in the master mode, one does not need to concern themselves with loss of lock since the reference clock and the VCO clock are collocated on the die, and therefore experience the same thermal shift. Hence in master mode, once lock is initially acquired, it is not lost and no blanking of the display occurs.

The duty cycle of the PWM in both master and slave mode is set using a second register on the  $1<sup>2</sup>C$  interface.

An external PWM signal can also be applied in the PWM pin. This pin is AND'ed with the internal signal, giving the ability to control the duty cycle either via  $I^2C$  or externally by setting any of the 2 signals to 100% duty cycle.

#### **MANUAL MODE**

The 34844A can also be used in Manual mode without using the  $I^2C$  interface. By setting the pin M/ $\sim$ S High, the LED dimming will be controlled by the external PWM signal. The over-voltage protection limit can be settled by a resistor divider or a zener diode on A0/SEN pin.

During manual mode, all internal Registers are in Default Configuration, refer [Table](#page-49-0) 14, under this configuration the PIN and NIN pins are enabled to scale the current capability per string and may be disable by setting 2.2 V in the corresponding terminal.

Also in this mode, the device can be enabled as follows:

• EN pin + PWM signal (Two Signals):

In this configuration, the PWM signal applied to PWM pin will be in charge of controlling the LED dimming and a second signal will enable or disable the chip through the EN pin.

• PWM Signal tied to SDA pin (Just ONE signal):

In this configuration the PWM pin should be tied to the SDA pin. The PWM signal applied to PWM pin will be in

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charge of controlling LED dimming and enabling the device every time the PWM is active. For this configuration the EN pin should be LOW.

### *I2C BUS SPECIFICATION*

The 34844A is a unidirectional device that can only be written by an external control unit. Since the device is a 7 bit address device (1110110), the control unit needs to follow a specific data transfer format which is shown in [Table](#page-48-0) 26.



#### **Figure 26. A Complete Data Transfer**

<span id="page-48-0"></span>For a complete data transfer, please use this format in the following order:

- 1. START condition
- 2. 34844A device address and Write instruction (R/W = 0)
- 3. First data pack, it corresponds to the 34844A register that needs to be written. (refer to [Table](#page-49-1) 13)
- 4. Second data pack, it corresponds to the value that should be written to that register. (refer to **[Table](#page-49-1) 13)**
- 5. STOP condition

I<sup>2</sup>C variables description:

- START: this condition occurs when SDA changes from HIGH to LOW while SCK is HIGH.
- ACKNOWLEDGE: The acknowledge clock pulse is generated by the Master (Control Unit).
- The transmitter releases the SDA line (HIGH) during the acknowledge clock pulse.The receiver (34844A) must pull

down the SDA line during this acknowledge pulse to indicate that the data was correctly written.

• Bits in the first byte: The first seven bits of the first bite make up the slave address. The eighth bit is the LSB (least significant bit), which determines the direction of the message (Write = 0)

For the 34844A device, when an address is sent, each of the devices in a system compares the first seven bits after the START condition with its address. If they match, the device considers itself addressed by the control unit as a slave-receiver.

STOP: this condition occurs when SDA changes from LOW to HIGH while SCK is HIGH

For more information about "I<sup>2</sup>C BUS SPECIFICATION" please refer to the following link:

http://www.nxp.com/acrobat\_download/literature/ 9398/39340011.pdf

## *LOGIC COMMANDS AND REGISTERS*

#### <span id="page-49-1"></span>**Table 13. Write Registers**



All registers and POWER ON/OFF channels should be reconfigured every time the part gets recovered from a POR or shutdown condition.

The configuration sequence every time the part is power up should be as follows:

- 1. Take the PWM pin low
- 2. Power up the part
- 3. Configure all registers
- 4. Take the PWM pin High



#### <span id="page-49-0"></span>**Table 14. Register Description**

For configuring the part once in operation it is

Special considerations should be taken for re-configuring POWER ON/OFF functions, please refer to the [POWER OFF](#page-45-0) 

recommended to follow this sequence:

[and POWER ON LED CHANNELS](#page-45-0) section.

1. Take the PWM pin low 2. Configure the registers 3. Take the PWM pin High



### **Table 14. Register Description**

**Table 15. Over-voltage Protection**



# **TYPICAL APPLICATIONS**



 **Figure 27. Manual Mode (Single Wire Control) Conditions: VIN = 24 V, VOUT = 47 V, Load = 16S10P, ILED = 60 mA, OVP = 53V, fSW = 300 kHz**



 **Figure 28. Manual Mode (Two Wire Control) Conditions:**  $V_{IN}$  = 24 V,  $V_{OUT}$  = 47 V, Load = 16S10P,  $I_{LED}$  = 60 mA, OVP = 53V,  $f_{SW}$  = 300 kHz



 **Figure 29. I2C (Master Mode) Conditions: VIN = 24 V, VOUT = 47 V, Load = 16S10P, ILED = 60 mA, OVP = 53V, fSW = 300 kHz**



 **Figure 30. I2C (Slave Mode) Conditions:**  $V_{IN}$  = 24 V,  $V_{OUT}$  = 47 V, Load = 16S10P,  $I_{LED}$  = 60 mA, OVP = 53V,  $f_{SW}$  = 300 kHz

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## TYPICAL APPLICATIONS



 **Figure 31. HIGH VOUT application (Manual Mode) Conditions: VIN = 60 to 72V, VOUT = 120 V, Load = 40S8P, ILED = 60 mA, OVP = 125 V, fSW = 300 kHz**

## **COMPONENTS CALCULATION**

<span id="page-54-0"></span>The following formulas are intended for the calculation of all external components related with the Boost converter and Network compensation.

In order to calculate a Duty Cycle, the internal losses of the MOSFET and Diode should be taken into consideration.

$$
D = \frac{Vout + V_D - Vin}{Vout + V_D - V_{SW}}
$$

The average input current depends directly to the output current when the internal switch is off.

$$
Iin_{avg} = \frac{Iout}{1 - D}
$$

#### **Inductor**

For calculating the Inductor we should consider the losses of the internal switch and winding resistance of the inductor.

$$
L = \frac{(Vin - V_{SW} - (Iin_{avg} \times rw)) \times D}{Iin_{avg} \times r \times F_{SW}}
$$

It is important to look for an inductor rated at least for the maximum input current.

$$
Iin_{max} = Iin_{avg} + \frac{Vin \times (Vout - Vin)}{2 \times L \times F_{SW} \times Vout}
$$

#### **Input Capacitor**

The input capacitor should handle at least the following RMS current.

$$
Irms_{\text{Cin}} = \left(\frac{\text{Vin} \times (\text{Vout} - \text{Vin})}{2 \times L \times F_{\text{SW}} \times \text{Vout}}\right) \times 0.3
$$

## $CSG = A_{CSA} \times R_{Sense}$

$$
Cout = \frac{R_{Comp} \times 5 \times G_M \times Iout \times L}{(1 - D) \times Vout \times CSG}
$$

The output voltage ripple  $(\Delta V_{\text{OUT}})$  depends on the ESR of the Output capacitor, for a low output voltage ripple it is recommended to use Ceramic capacitors that usually have very low ESR. Since ceramic capacitor are expensive, Electrolytic or Tantalum capacitors can be mixed with ceramic capacitors to have a cheaper solution.

$$
ESR_{Cout} = \frac{Vout \times \Delta Vout \times F_{SW} \times L}{Vout \times (1 - D)}
$$

The output capacitor should handle at least the following RMS current.

#### **Network Compensation**

Since this Boost converter is current controlled, Type II compensation is needed.

$$
Irms_{\text{Cout}} = \text{Iout} \times \sqrt{\frac{\text{D}}{1-\text{D}}}
$$

I order to calculate the Network Compensation, first we need to calculate all Boost Converter components.

For this type of compensations we need to push out the Right Half Plane Zero to higher frequencies where it can't affect the overall loop significantly.

$$
f_{RHPZ} = \frac{Vout \times (1 - D)^2}{Iout \times 2 \times \pi \times L}
$$

The Crossover frequency must be set much lower than the location of the Right half plane zero

$$
f_{Cross} = \frac{f_{RHPZ}}{5}
$$

Since our system has a fixed Slope compensation set by R<sub>SLOPE</sub>, R<sub>COMP</sub> should be fixed for all configurations.

$$
R_{Comp} = 5.6 \text{kohm}
$$

 $C_{COMP1}$  and  $C_{COMP2}$  should be calculated as follows:

#### **Output Capacitor**

For the output capacitor selection the internal current sense gain (CSG) and the Transconductance should be taken in consideration.

The CSG is the internal  $R_{\text{SENSE}}$  times the current sense amplifier gain  $(A_{CSA})$ .

$$
C_{\text{Comp1}} = \frac{2}{f_{\text{Cross}} \times R_{\text{Comp}} \times \pi \times 2}
$$

$$
C_{Comp2} = \frac{G_M}{6.28 \times F_{SW}}
$$

In order to improve the transient response of the boost, on the 34844A, a resistor divider has been implemented from the PWM pin to ground with a connection to the compensation network. This configuration should inject a 1.0 V signal to the COMP pin and the Thevenin-equivalent resistance of the divider is close to RCOMP, i.e.  $R_{\text{COMP}} = 6.8 \text{ k}$ and  $R_{PCOMP}$ = 27 k for a 5.0 V PWM signal.



#### **Slope Compensation**

Slope Compensation can be expressed either in terms of Ampers/Second or as Volts/Second, through the use of the transfer resistance.

The following formula express the Slope Compensation in terms of V/μs:

$$
V_{SLOPE} = \frac{(Vout-Vin) \times CSG}{L \times 2}
$$

Where "L" is in μH

In order to have this slope compensation, the following resistor should be set.

$$
R_{\text{SLOPE}} = \frac{33 \times 10^3}{V_{\text{SLOPE}} \times 5}
$$

**Variable Definition** D= Boost Duty Cycle  $V_{\text{OUT}}$ = Output Voltage  $V_D$ = Diode Forward Voltage V<sub>IN</sub>= Input Voltage V<sub>SW</sub>= V<sub>DROP</sub> of Internal Switch ΔV<sub>OUT</sub>= Output Voltage Ripple Ratio IINAVG= Average Input Current  $I<sub>OUT</sub> = Output Current$ r=Input Current Ratio  $IIN_{MAX}$ = Maximum input current IRMS<sub>CIN</sub>= RMS current for Input Capacitor  $IRMS<sub>COUT</sub>$ = RMS current for Output Capacitor L= Inductor  $R_W$ = Inductor winding DC Resistance f<sub>SW</sub>= Boost Switching Frequency CSG= Current Sense Gain = 0.2 V/A  $A<sub>CSA</sub>$ = Current Sense Amplifier Gain = 9 R<sub>SENSE</sub>= Current Sense Resistor = 22mohm  $C<sub>OUT</sub> = Output Capacitor$ R<sub>COMP</sub>= Compensation Resistor  $G_M$ = OTA Transconductance  $ESR<sub>COUT</sub> = ESR of Output Capacitor$ f<sub>RHPZ</sub>= Right Half Plane Zero Frequency f<sub>CROSS</sub>= Crossover Frequency C<sub>COMP1</sub>= Compensation Capacitor C<sub>COMP2</sub>= Shunt Compensation Capacitor  $V_{SI,OPF}$ = Slope Compensation (V/ $\mu$ s)  $R_{SI, OPF}$ = External Resistor for Slope Compensation

# **LAYOUT GUIDELINES**

### **RECOMMENDED STACK-UP**

The following table shows the recommended layer stackup for the signals to have good shielding and Thermal Dissipation.





### **DECOUPLING CAPS**

It is recommended to place decoupling caps of 100 pf at the beginning and at the end of any power signal traces to filter high frequency noise.

Decoupling caps of 100 pf should be also placed at the end of any long trace to cancel antenna effects on it.

These caps should be located as closed as possible to the point to be decoupled and the connection to GND should be as short as possible.

### **SM-BUS/I2C COMMUNICATION AND CLOCK SIGNALS (SDA, SCK AND CK)**

To avoid contamination of these signals by nearby high power or high frequency signals, it is a good practice to shield them with ground planes placed on adjacent layers. Make sure the ground plane is uniform through the whole signal trace length.



#### **Figure 32. Recommended shielding for critical signals.**

These signals shall not run parallel to power signals or other clock signals in the same routing layer. If they have to cross or to be routed close to a power signal, it is a good practice to trace them perpendicularly or at 45° on a different layer to avoid coupling noise.

#### **SWITCHING NODE (SWA & SWB)**

The components associated to this node must be placed as close as possible to each other to keep the switching loop small enough so that it does not contaminate other signals. However, care must be taken to ensure the copper traces used to connect these components together on this node are capable to handle the necessary current and voltage.

As a reference, a 10 mils trace with a thickness of 1.0 oz. of copper is capable of handling one ampere.

Traces for connecting the inductor, input and output caps should be as wide and short as possible to avoid adding inductance or resistance to the loop. The placement of these components should be selected far away from sensitive signals like compensation, feedback and internal regulators to avoid power noise coupling.

### **COMPENSATION COMPONENTS**

Components related with COMP pin need to be placed as close as possible to the pin.

### **FEEDBACK SIGNAL**

The trace of the feedback signal (VOUT) should be routed perpendicularly or at 45° on a different layer to avoid coupling noise, preferably between ground or power planes.



 **Figure 33. Feedback Signal Tracing**

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# **PACKAGING**

### *PACKAGE DIMENSIONS*

For the most current package revision, visit **[www.freescale.com](http://www.freescale.com)** and perform a keyword search using the "98A" listed below.





**EP SUFFIX** 32-PIN 98ASA10800D REVISION O

**34844**



DETAIL M<br>PIN 1 BACKSIDE IDENTIFIER





**EP SUFFIX** 32-PIN 98ASA10800D REVISION O



#### NOTES:

- 1. ALL DIMENSIONS ARE IN MILLIMETERS.
- 2. DIMENSIONING AND TOLERANCING PER ASME Y14.5M-1994.
- RADIUS ON TERMINAL IS OPTIONAL.  $\overline{3}$ .
- $\mathcal{A}$ COPLANARITY APPLIES TO LEADS, AND DIE ATTACH PAD.
- 5. MINIMUM METAL GAP SHOULD BE 0.2 MM.



**EP SUFFIX** 32-PIN 98ASA10800D REVISION O



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